

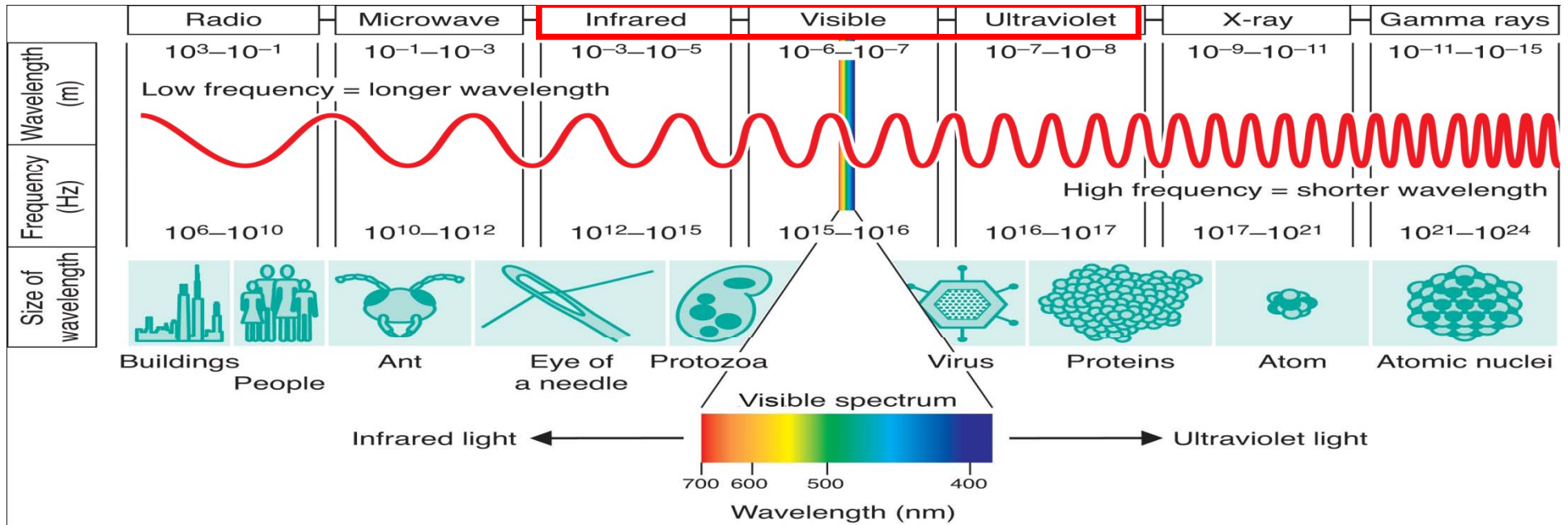
# Lidar Technique: Basic Hardware Components (Lasers and Electronics)

**Prof. Dr. Alex Papayannis**

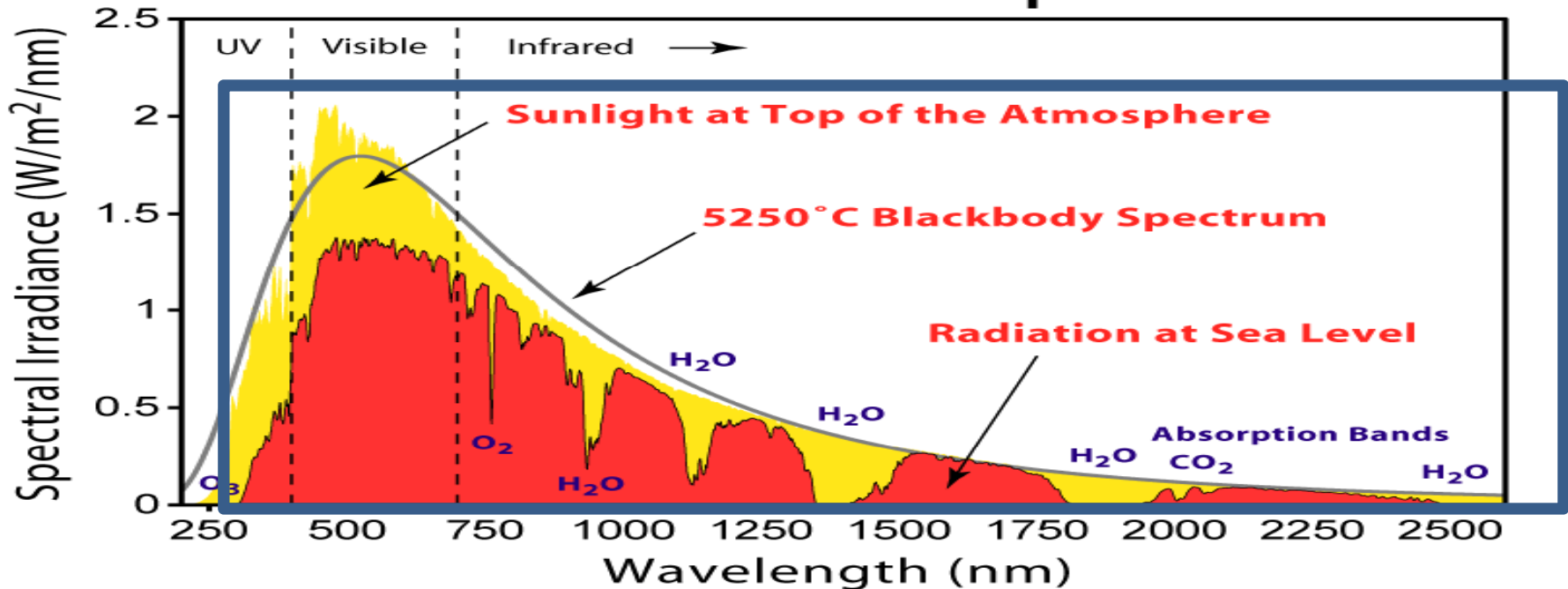
Head of the Laser Remote Sensing Unit (LRSU)  
National Technical University of Athens, Greece

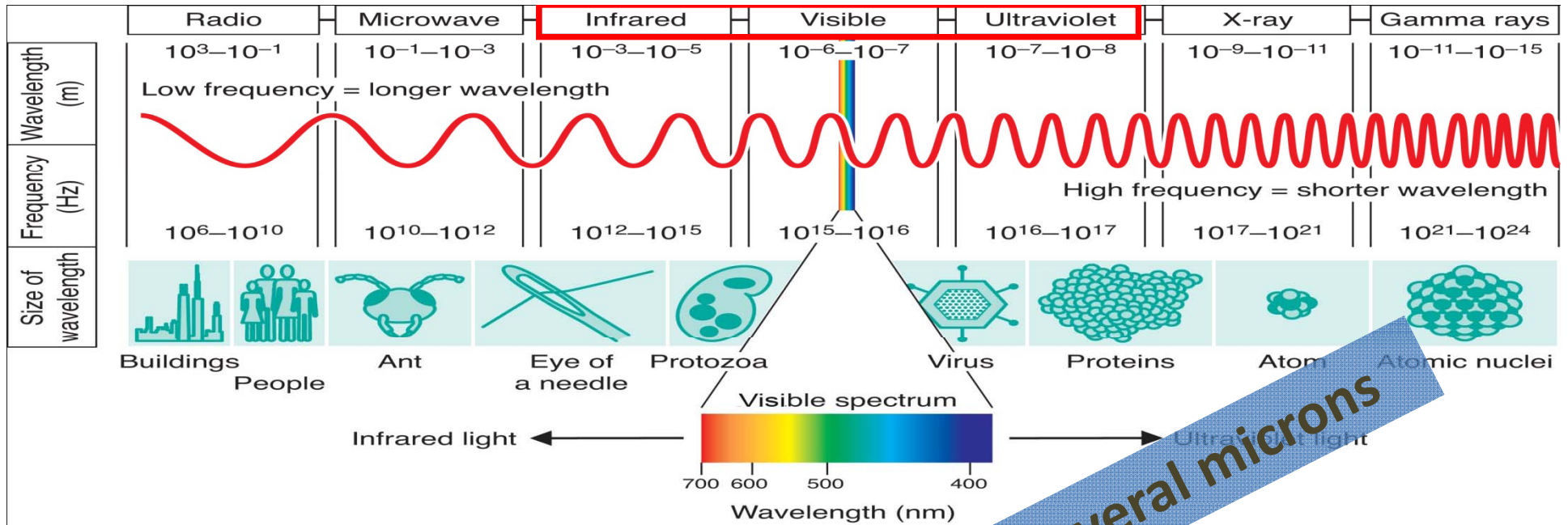
Website: <http://lrsu.physics.ntua.gr/en>

Email: [apdlidar@central.ntua.gr](mailto:apdlidar@central.ntua.gr)

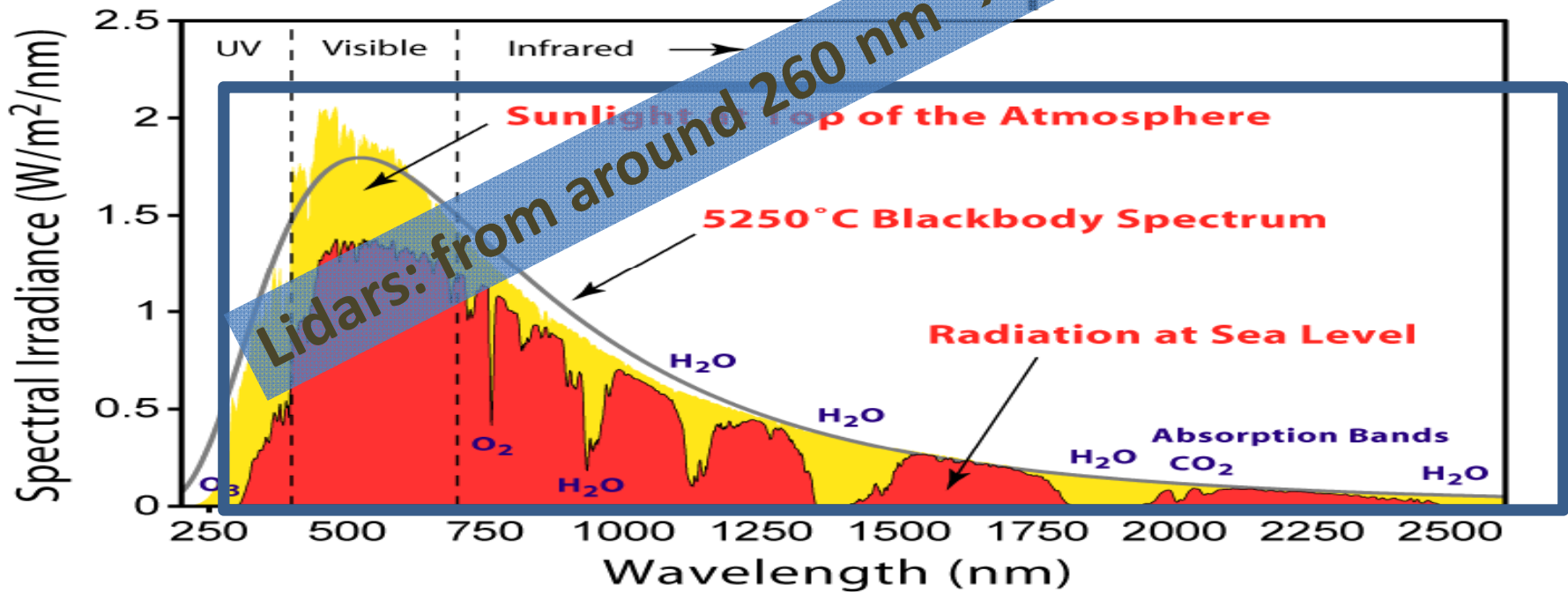


## Solar Radiation Spectrum





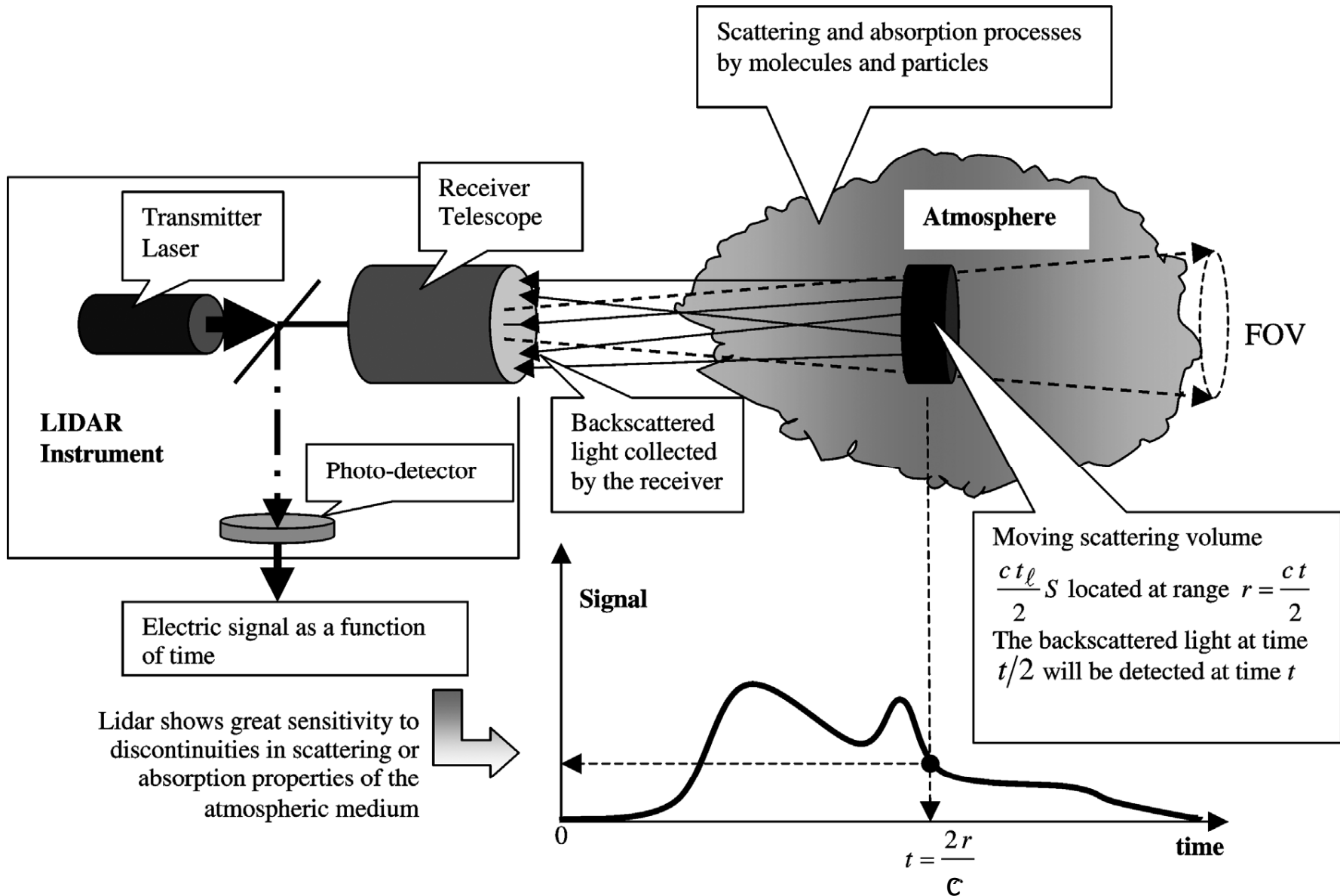
## Solar Radiation Spectrum





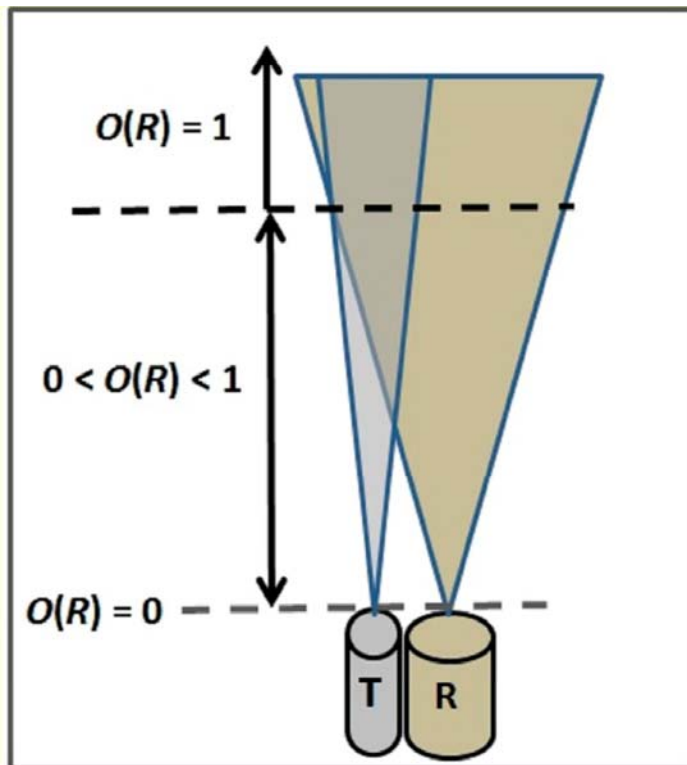


# Typical LIDAR Experimental Set-up



# The Lidar Principle

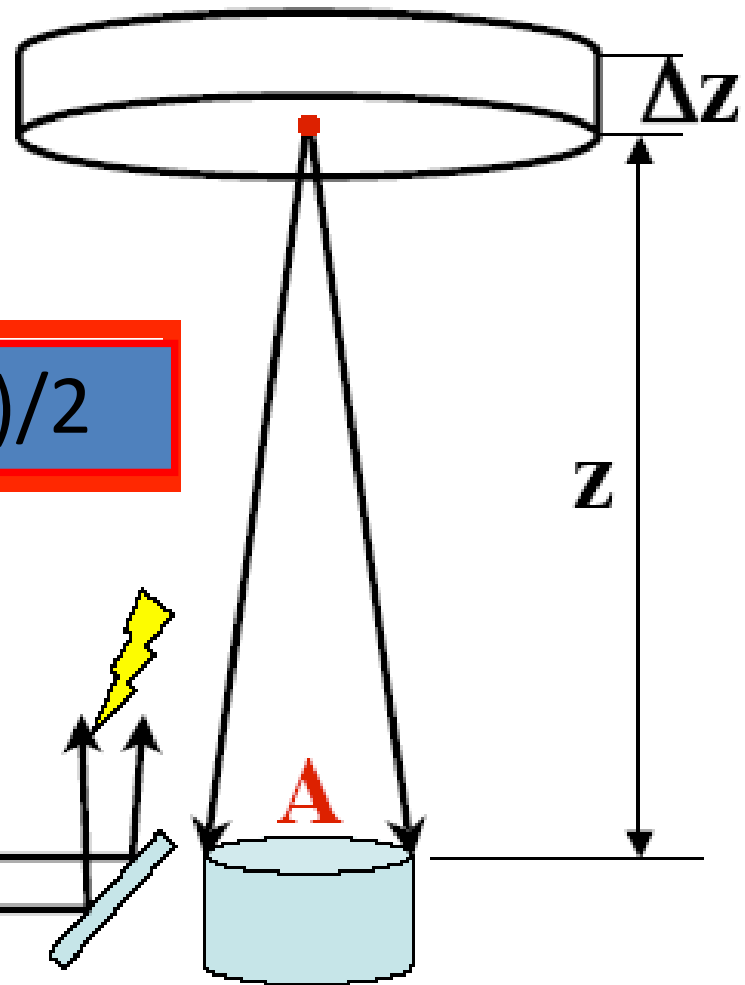
$\Delta t^* = 1/F_D$ ,  $F_D$  = Signal sampling frequency (10-40 MHz  $\rightarrow$   $\sim$ GHz),  $\Delta z$  = range resolution



**O(R)**: Overlap function  
**T**: Laser (Emitter)  
**R**: Telescope (Receiver)

$$\Delta z = c (\Delta t^*) / 2$$

**Pulsed  
Laser**



Lidar signal  $S(z) \sim 1/z^2$

# Lidar System Components

## General physical properties:

- LIDAR: robust, compact, low power consumption, stability (alignment/optics/mechanical structure), low weight (airborne/space borne systems), easy to operate, 24/7 operationality, remote control, low-cost maintenance-operation,
- Housing: temperature-humidity controlled housing, compact with protection window, indirect solar radiation, weather-proof,
- Transportable (special campaigns).

## Transmitter (Laser):

- Single-wavelength & polarized laser beam
- High energy laser source
- Wavelength: 0.266-10.6  $\mu\text{m}$  (several wavelengths - tunable for special cases)
- High repetition rates (desired): several Hz to 20 some kHz.

## Safety (laser Beam):

Eye-safe emission (exiting the protective window): Use convenient wavelengths + beam expander!

## Operation Mode:

- Day/nighttime, continuous, automated operation
- Time resolution (several seconds to minutes)
- Spatial resolution ( $\sim 15\text{-}100$  m or better, depending on height)

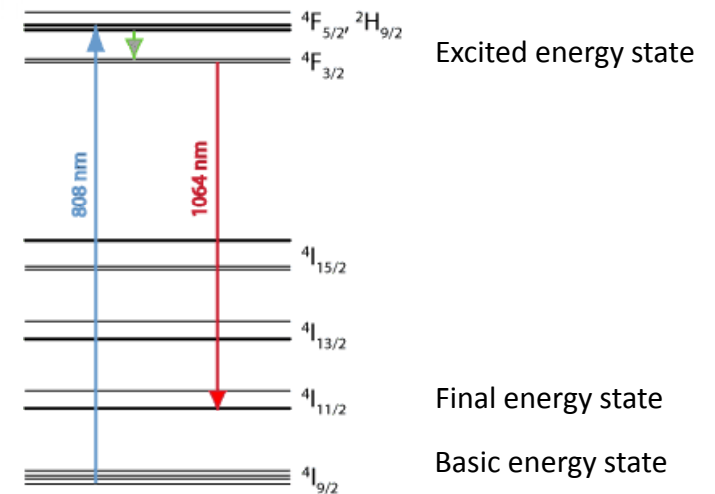
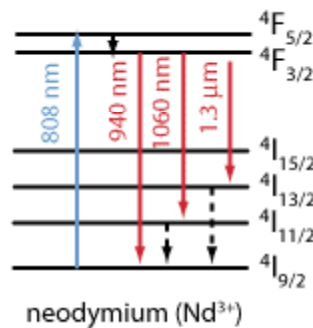
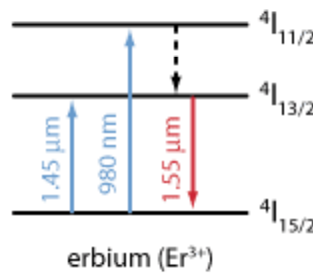
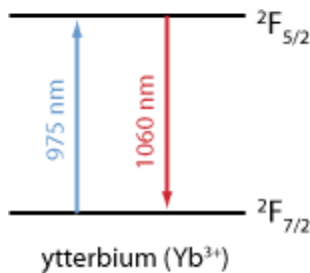
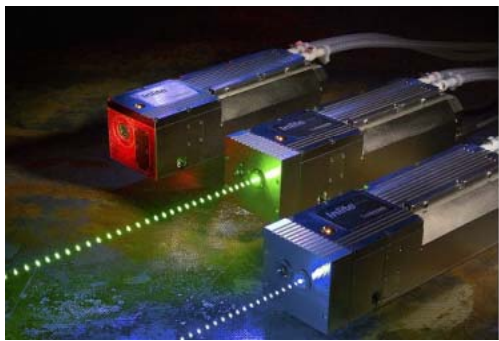
## Signal Received:

- Backscatter (molecules + aerosols)
- Atmospheric Background correction (averaged signal at high ranges)
- Electronic noise evaluation (use of pre-trigger)
- Depolarization channels

# Lidar System Components

## Laser Sources:

**Typical laser sources:** Nd:YAG (1.064 $\mu$ m), XeCl (0.308 $\mu$ m), Er:glass (1.54 $\mu$ m), Er:YAG (2.94 $\mu$ m), Tm,Ho:YAG (2 $\mu$ m), CO<sub>2</sub> (10.6  $\mu$ m), etc.



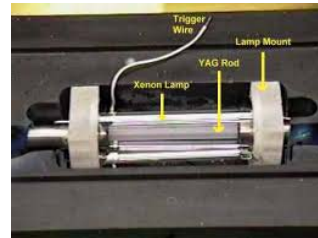
**Blue:** Pump optical beam (diode laser or flash lamp) **Red:** emitted laser beam



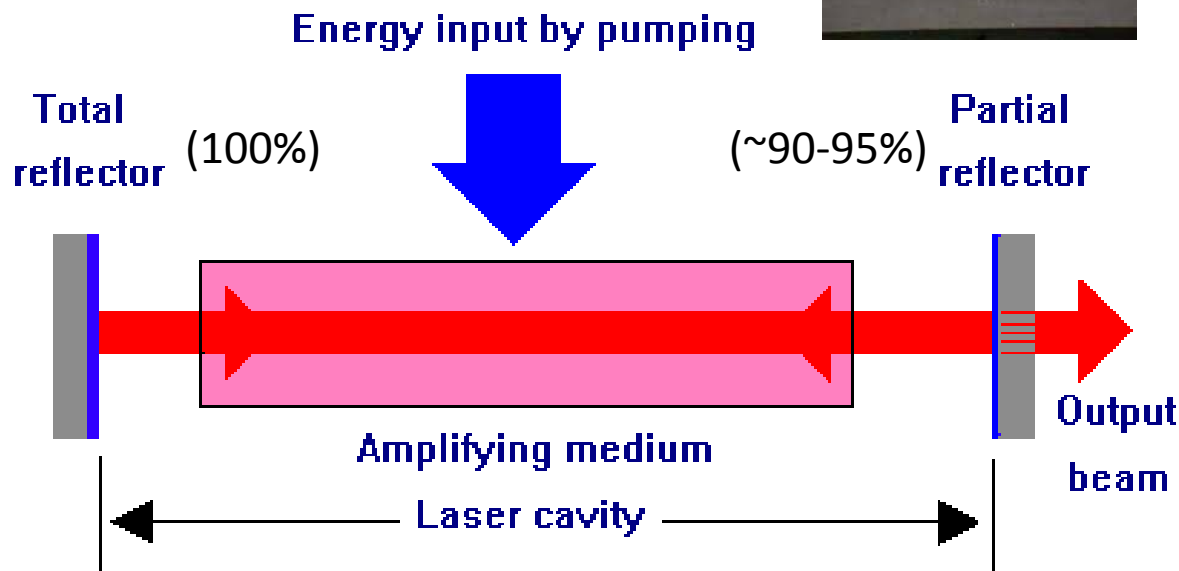


# Lidar System Components

## Laser Cavity (Type I-Solid state):



Laser crystals

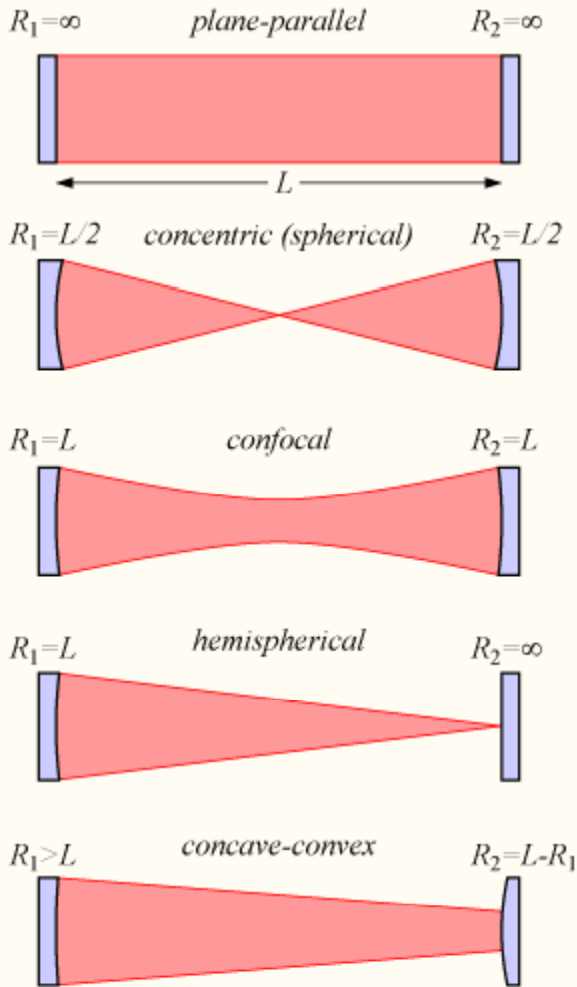


Nanosecond pulses  
Up to several Joules/pulse

Cavity reflectors

# Lidar System Components

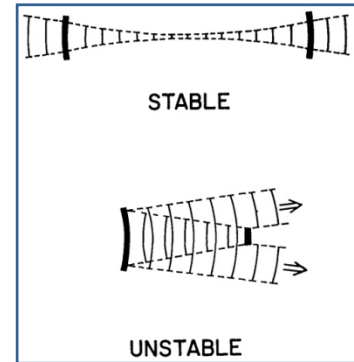
## Laser Cavity (Type I-Solid state):



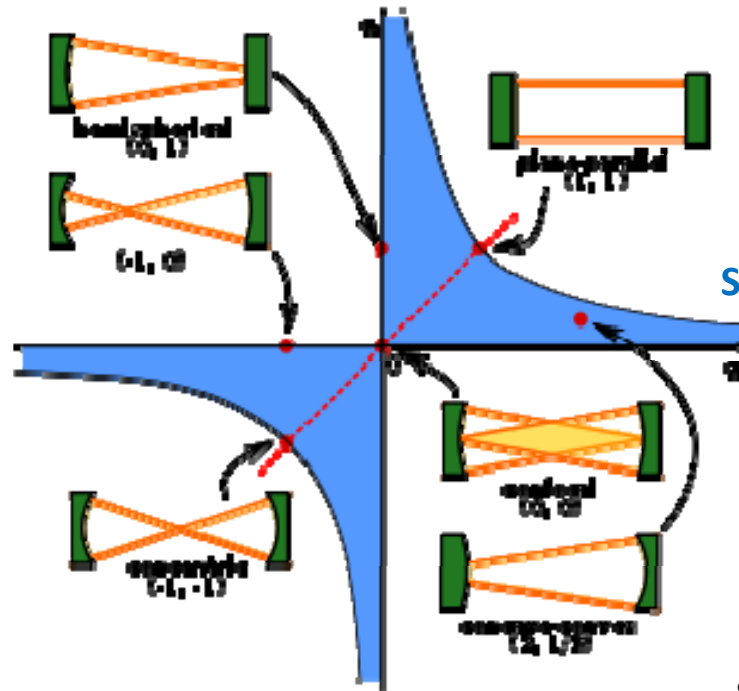
(Stability criterion)

$$0 \leq \left(1 - \frac{L}{R_1}\right) \left(1 - \frac{L}{R_2}\right) \leq 1.$$

$$g_1 = 1 - \frac{L}{R_1}, \quad g_2 = 1 - \frac{L}{R_2}$$



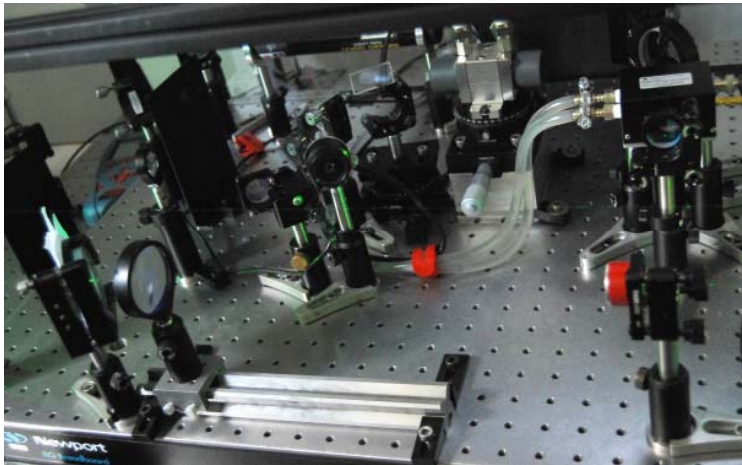
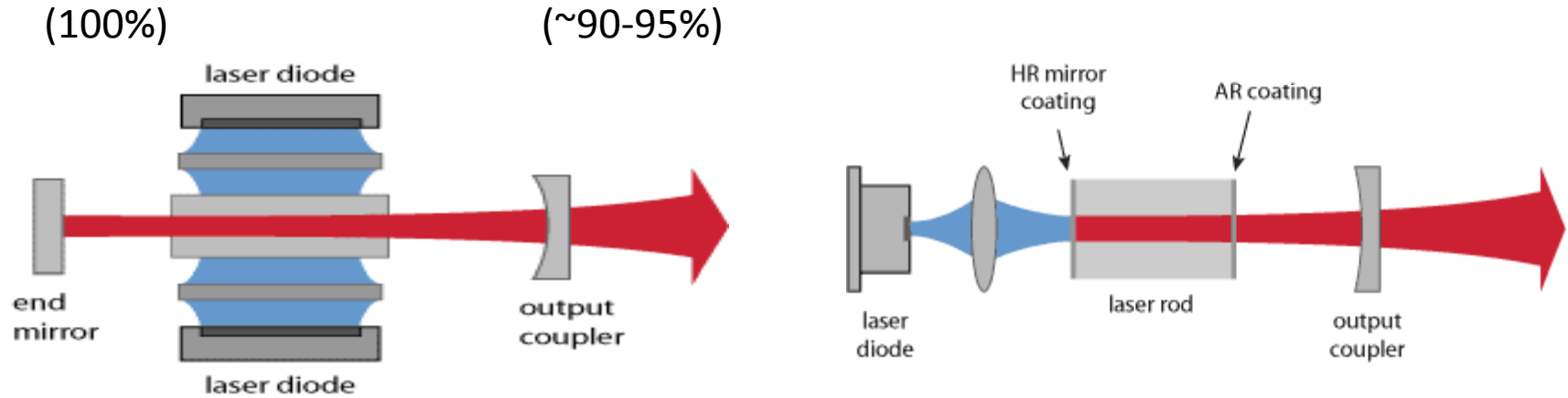
**Unstable:**  
After several round-trips the laser beams largely diverges



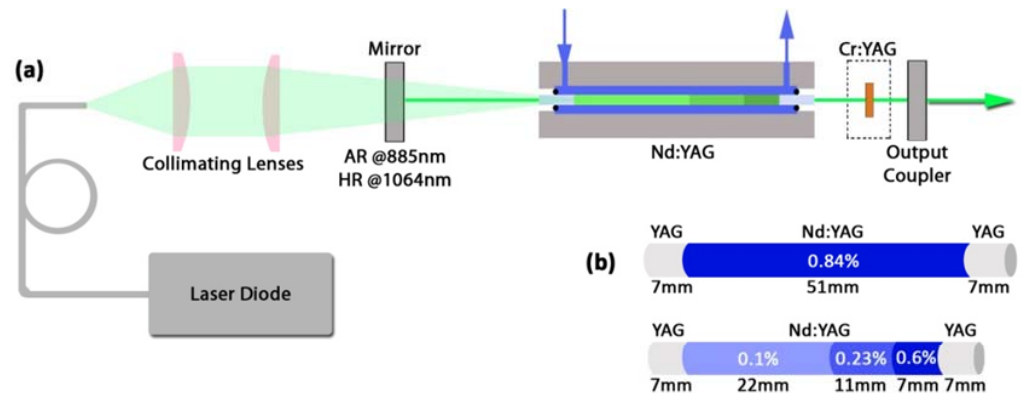
Siegman (1986)

# Lidar System Components

## Laser Cavity (Type IA-Diode pumped solid state lasers):



Diode pumped multi-segmented Nd:YAG laser developed for European Space Agency @ NTUA



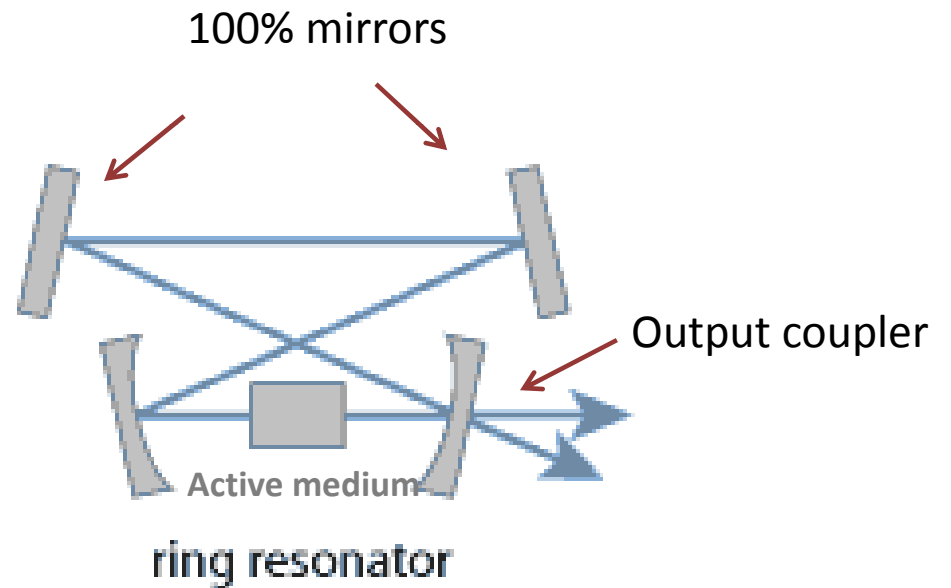
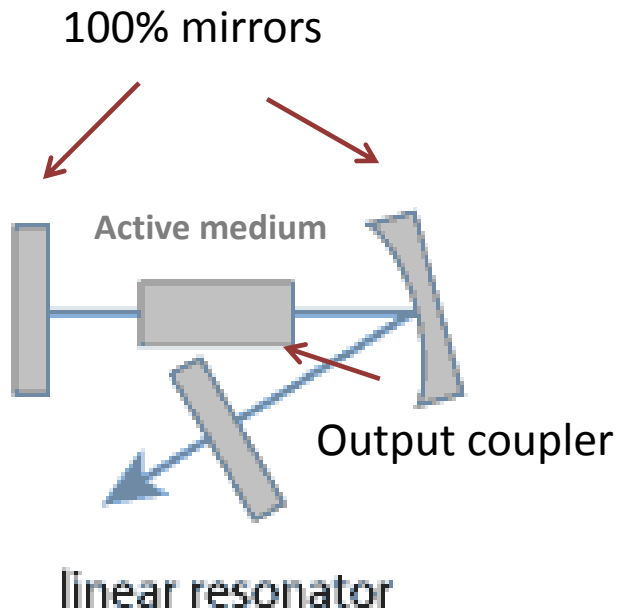
Nanosecond pulses  
Up to several Joules/pulse

Evangelatos et al. (2013; 2014)

# Lidar System Components

## Laser Cavity:

**Typical laser cavities:** (multiple beams passages between 100% reflection mirrors and output couplers)

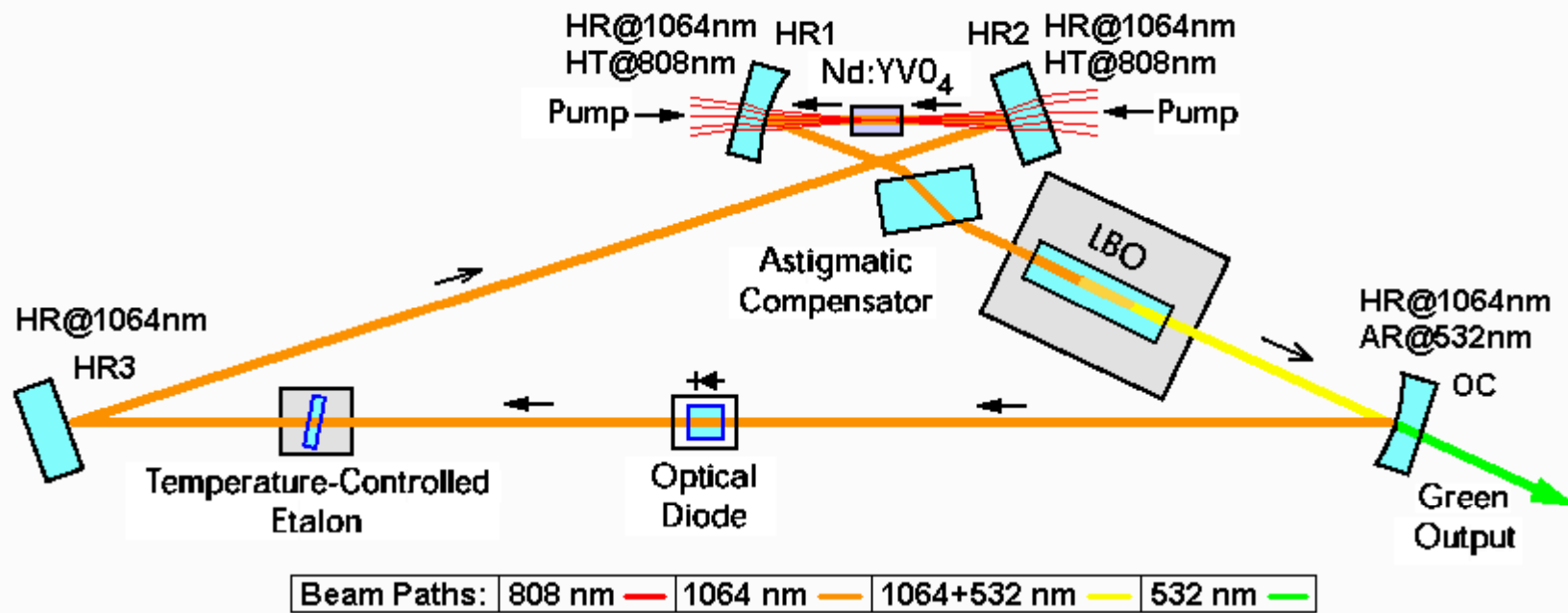




# Lidar System Components

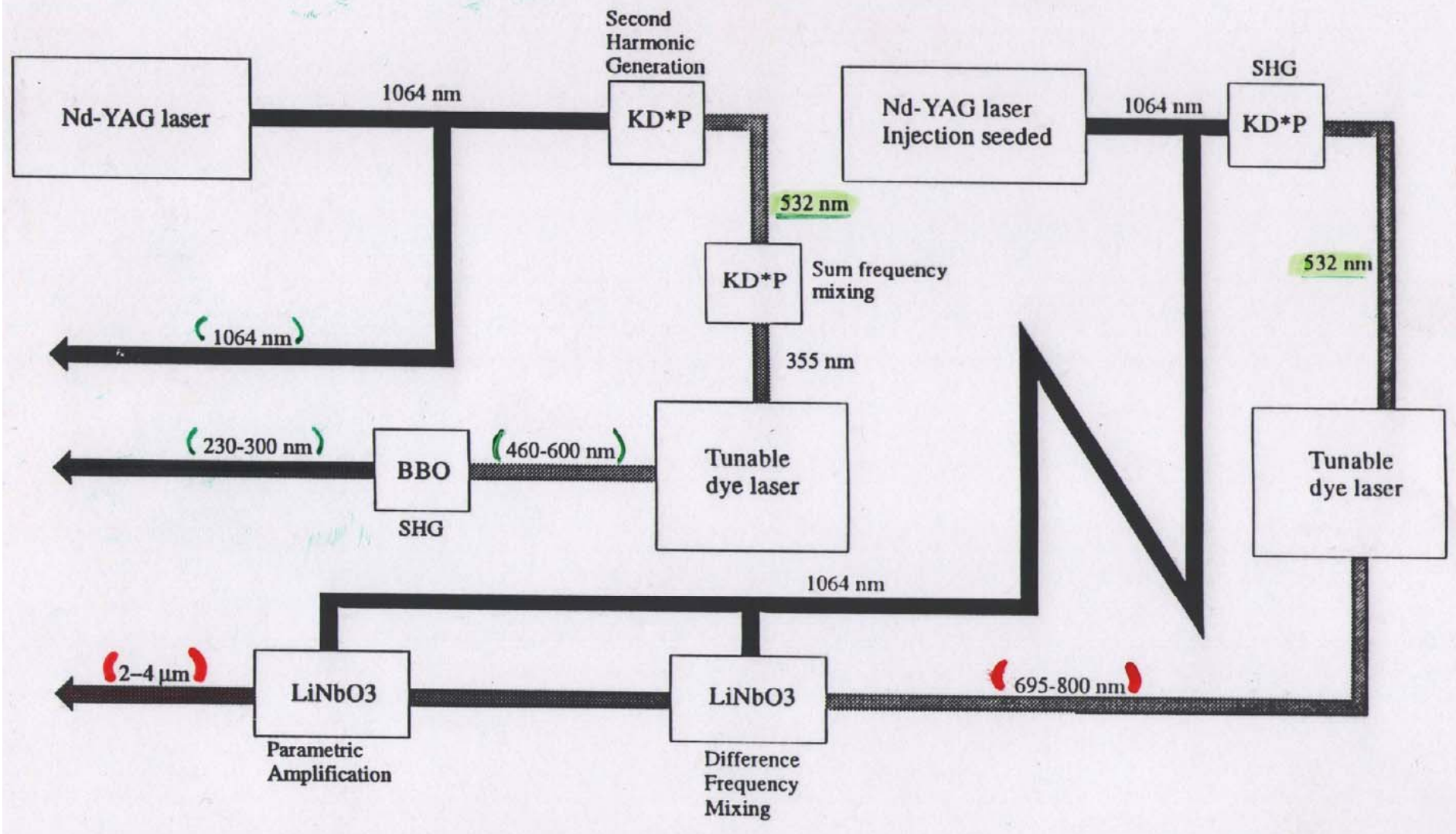
## Laser Cavity:

**Typical laser cavities:** (multiple beams passages between 100% reflection mirrors and output couplers)



Ring Cavity Resonator of Coherent, Inc. Verdi Green DPSS Laser

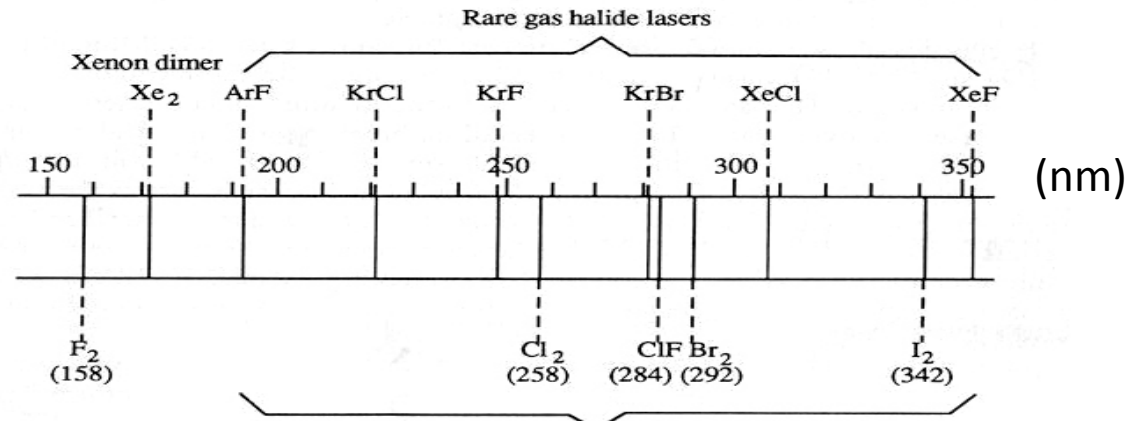
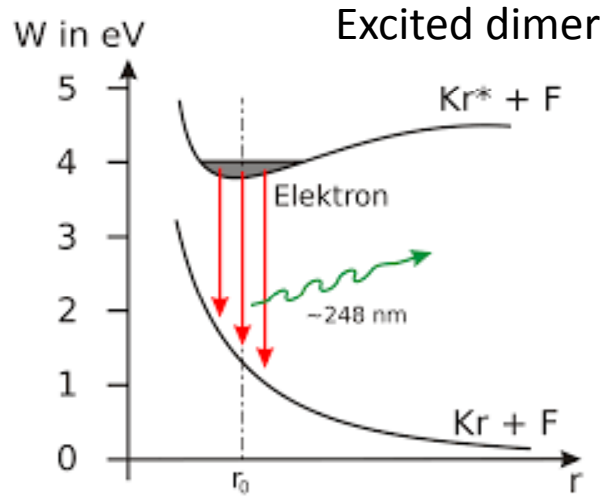
# Optical Sources used in the NPL Ultraviolet and Infrared DIAL System



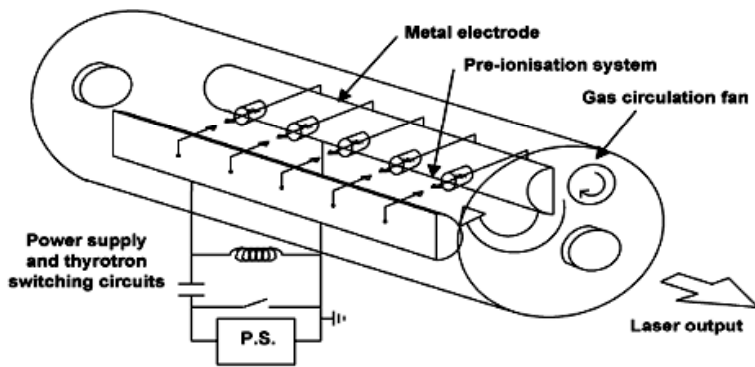
National Physical Laboratory (NPL), UK

# Lidar System Components

## Laser Cavity (Type II-Gas lasers-Excimer lasers):



de.wikipedia.org



www.photonicsolutions.co.uk

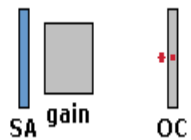
Nanosecond pulses  
 Up to several Joules/pulse  
 O<sub>3</sub> measurements (KrF+Raman, XeCl)

<http://www.twi-global.com/technical-knowledge/faqs/process-faqs/faq-what-is-an-excimer-laser/>

# Lidar System Components

## Laser Cavity (Type III-Femtosecond lasers):

Mode-locked lasers



Output  
laser  
beam

SA: Saturable absorber mirror

Gain medium

OC: output coupler

**Mode locking:** The laser resonator contains either an **active** element (an **optical modulator**) or a nonlinear **passive** element (a **saturable absorber**), which causes the formation of an ultrashort pulse circulating in the laser resonator.

**Passive mode-locking:** The gain medium compensates for losses, and the saturable absorber mirror (SA) enforces pulse generation. Each time the circulating pulse hits the output coupler mirror (OC), a pulse is emitted in the output.

**SA with very low losses at high energies!**

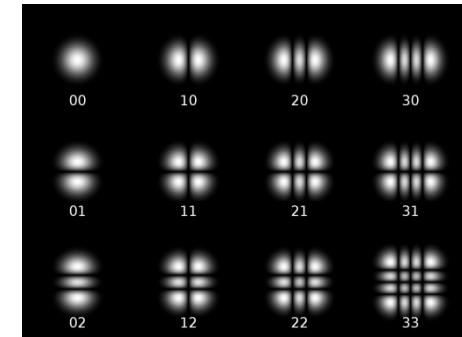
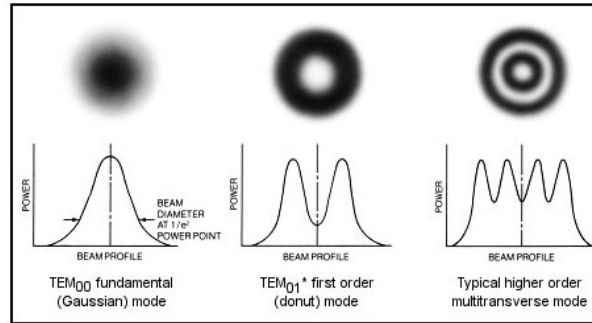
[www.rp-photonics.com](http://www.rp-photonics.com)



Femtosecond pulses  
Up to several mJ/pulse

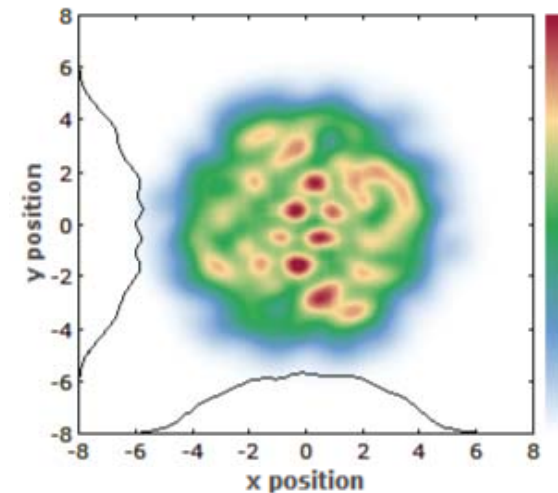
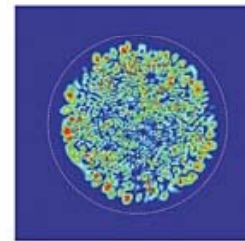
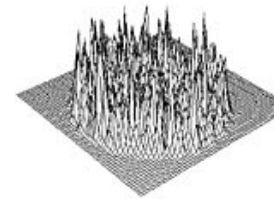
# Lidar System Components

## Laser Sources:



Transverse laser oscillating modes  
(inside the laser cavity)

### a) Multi-mode laser beams



[https://www.rp-photonics.com/beam\\_profilers.html](https://www.rp-photonics.com/beam_profilers.html)  
[www.spie.org](http://www.spie.org)

The laser energy is distributed over several oscillating “modes”, within the laser cavity

## Applications:

- Detection of aerosols, molecules, clouds, etc.

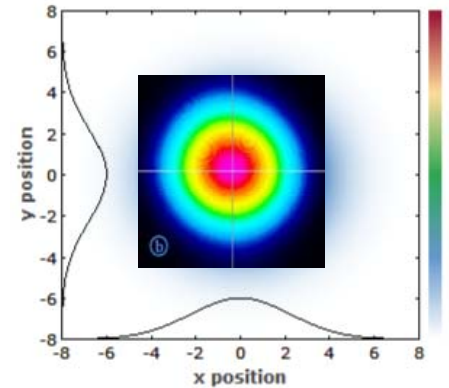


# Lidar System Components

## Laser Sources:

### b) Mono/Single-mode (single frequency): Injection seeded lasers

Evangelatos et al. (2013; 2014)



The laser energy is distributed over one single several oscillating “mode”, within the laser cavity

## Specs/Requirements:

-Very narrow laser linewidth (<1 MHz)

[@1.54  $\mu\text{m}$   $\rightarrow$  1.3 MHz Doppler shift  $\longleftrightarrow$  1 m/s wind velocity]

## Applications:

- Coherent transmitter in pulsed **Doppler** lidars (measurement of wind velocity + shear)
- High Spectral Resolution Lidars-**HSRL** (aerosol backscatter-extinction, wind velocity + shear)
- Temperature profiling, etc.

# Lidar System Components

## Common problems related to Laser Sources:

### a) Beam power instability (e.g. 266 nm)

Performance Specifications			
Wavelength	Pulse Width <sup>5</sup>	Short Term Energy Stability <sup>6</sup>	Long Term Power Drift <sup>7</sup>
1064 nm	8–12 ns	±2%	<3%
532 nm	1–2 ns <1064 nm	±3%	<5%
355 nm	2–3 ns <1064 nm	±4%	<6%
266 nm	3–4 ns <1064 nm	±8%	<10%

6. Pulse-to-pulse stability for >99% of pulses, measured over a 1 hour period.

7. Over 8 hour period with temperature variations of  $\pm 3^{\circ}\text{C}$ .

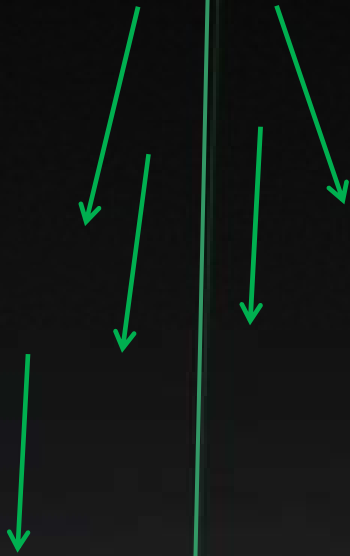
Source: Quanta Ray lasers (Spectra Physics)

### b) Earth problems (a good earthing is required)

### c) Stable input voltage is required

Laser Safety !





Received :  $\sim 10^m$  photons

$m \sim 0 - 10-15$  (depending on distance)

Emitted :  $10^n$  photons

$n \sim 10-20$



# Lidar System Components

## Photo-detectors (I)

### PhotoMultiplier Tubes (PMTs)

Spectral Range: 110 nm – 1200 nm [lidars: 247 up to ~880 nm]

[www.hamamatsu.com](http://www.hamamatsu.com)

Pros: Very good conversion efficiency

Cons: Only in the UV-VIS-beginning of NIR region



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## Photo-detectors (II)

### Avalanche PhotoDiodes (APDs)

Spectral Range:

APD-Si: 200 nm – 1100 nm

APD-Ge: 800-1550 nm

APD-InGaAs [lidars: 900-1500 nm]

Pros: Good conversion efficiency

Cons: Bulky, only in the near IR

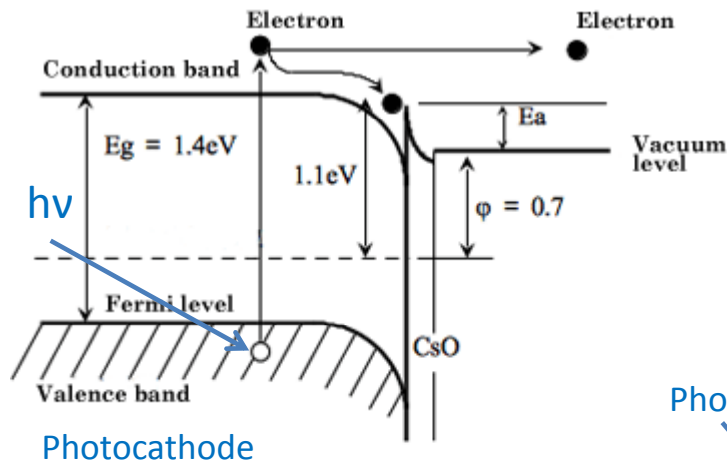
[www.hamamatsu.com](http://www.hamamatsu.com), [www.licel.com](http://www.licel.com)



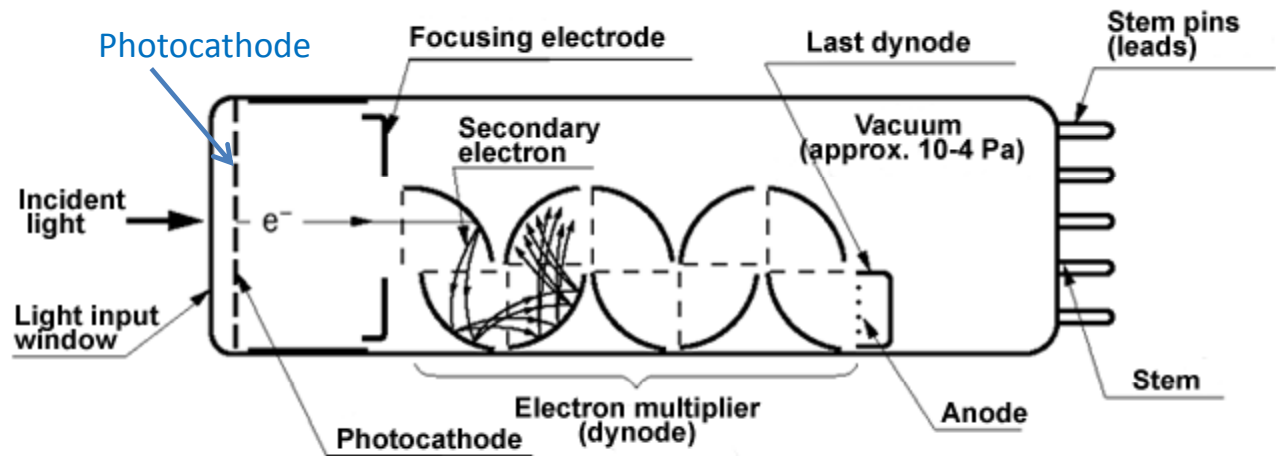
# Lidar System Components

## Photo-detectors (I)

### PhotoMultiplier Tubes (PMTs) – Operating Principle



[www.hamamatsu.com](http://www.hamamatsu.com)

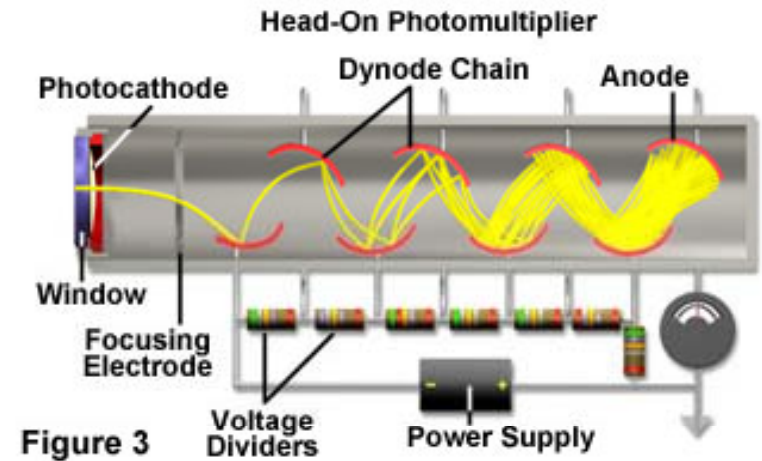
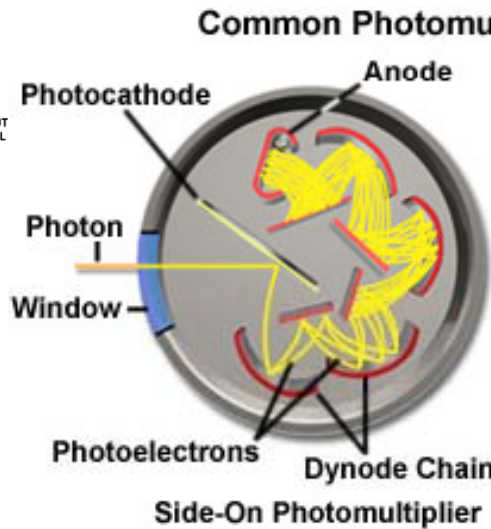
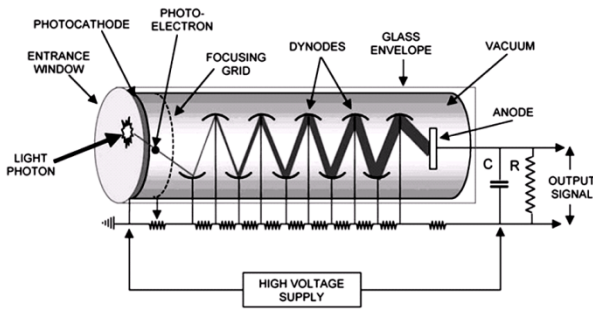




# Lidar System Components

## Photo-detectors (I)

### PhotoMultiplier Tubes (PMTs) - Operating Principle for detecting pulsed (lidar) signals

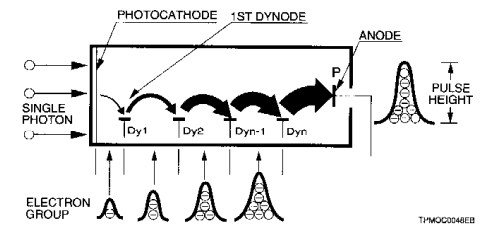


Side-on



Head-on

[www.olympusmicro.com](http://www.olympusmicro.com)

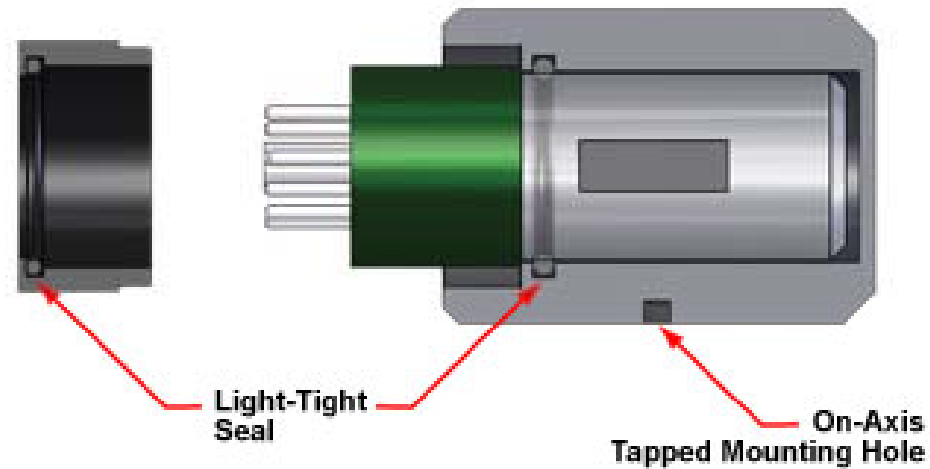


High voltage divider circuit: divide the high voltage (800-1000 V) to the dynodes

# Lidar System Components

## Photo-detectors (I)

### PhotoMultiplier Tubes (PMTs) - Housing



[www.thorlabs.com](http://www.thorlabs.com)

A proper metallic housing (magnetic shielding) is required to protect the very sensitive PMT from :

- external EM fields
- ambient temperature
- humidity

# Lidar System Components

## Photo-detectors (I)

### PhotoMultiplier Tubes (PMTs) – Photocathode materials

The response of a PMT is specified by the **photocathode sensitivity**:

- **Quantum efficiency (%)**:

$QE = \frac{\text{Nphotoel. emitted by the photocathode}}{\text{Number incident photons}}$

- **Cathode radiant sensitivity (mA/W)**:

Photocurrent produced (mA) in response to the incident light power (W)

$QE(\%) = [124/\lambda(\text{nm})] * \text{radiant sensitivity (mA/W)}$

- **Cathode luminous sensitivity ( $\mu\text{A/lm}$ )**:

It relates the photocathode current to the human eye response

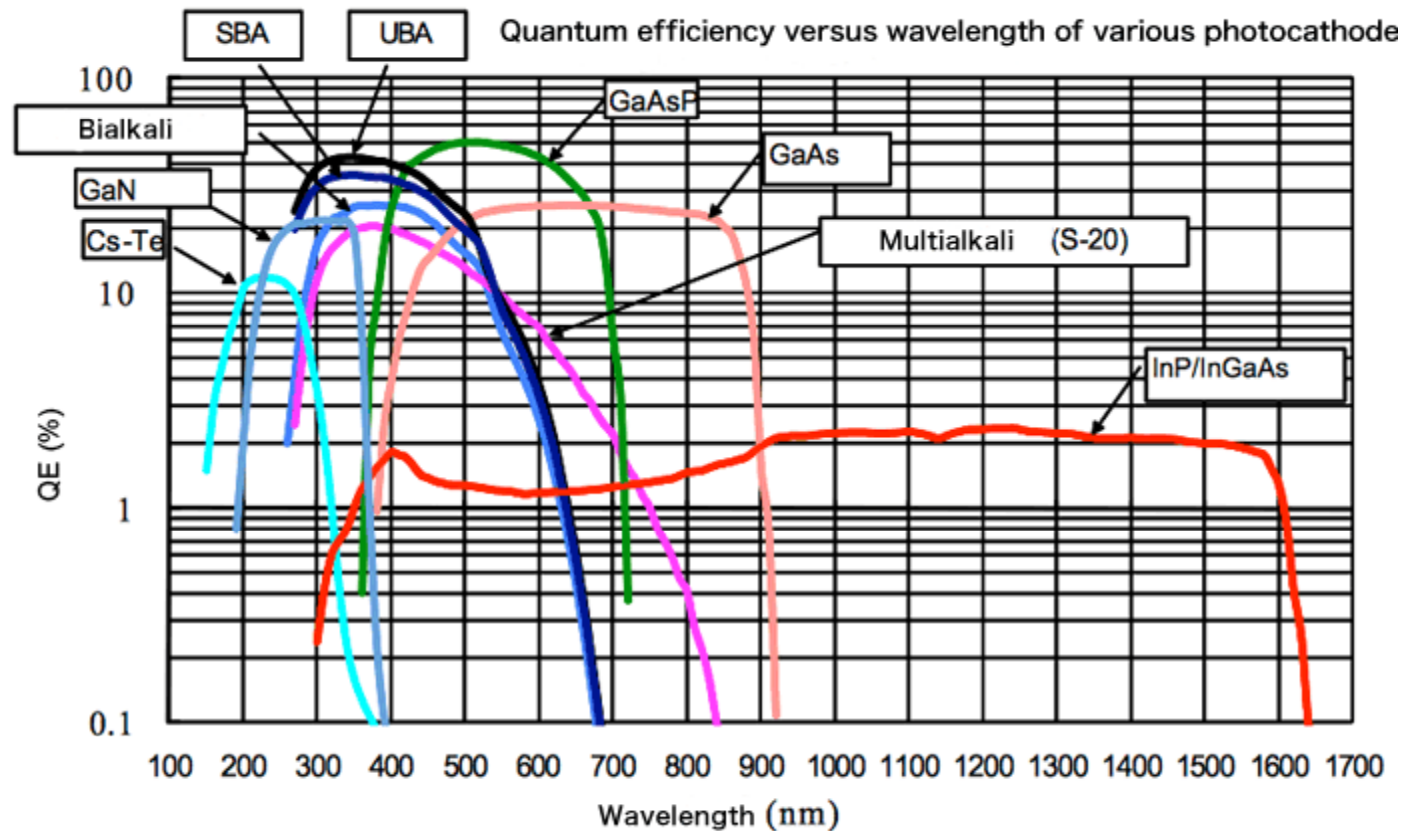
Current produced by an incident flux of 1 lumen from a Tungsten filament source (@2856 K)

# Lidar System Components

## Photo-detectors (I)

### PhotoMultiplier Tubes (PMTs) – Photocathode materials

The response of a PMT is specified by the photocathode sensitivity

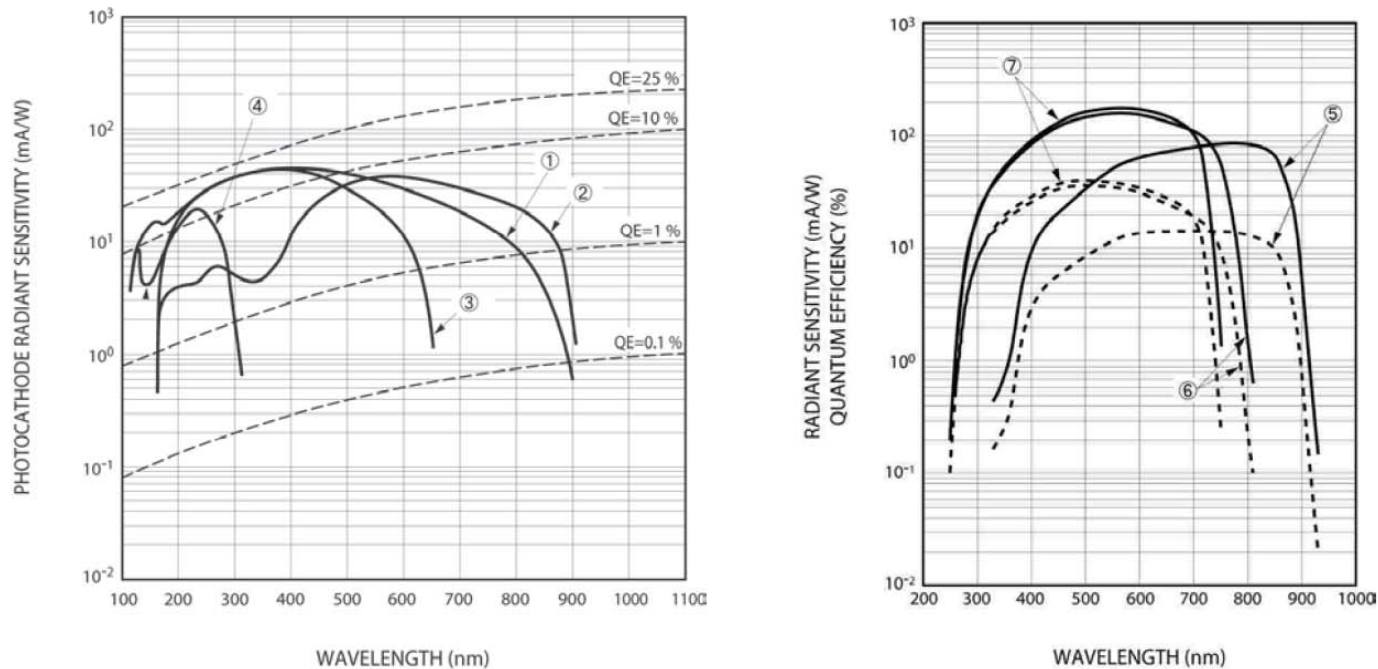


# Lidar System Components

## Photo-detectors (I)

### PhotoMultiplier Tubes (PMTs) - Photocathode

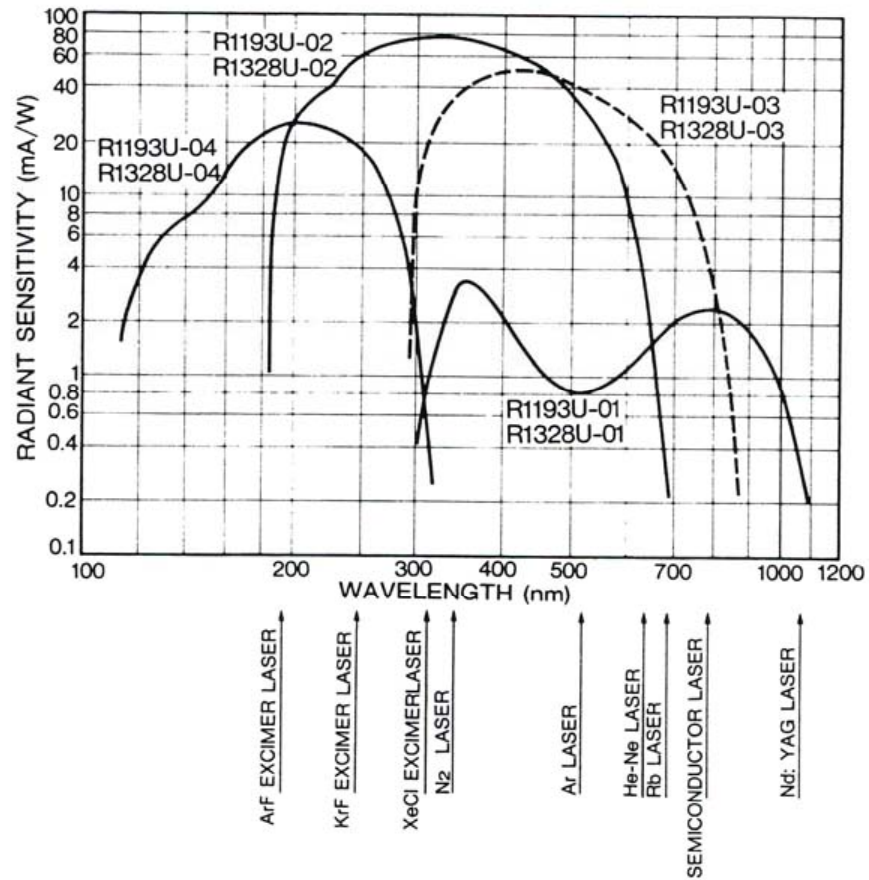
Figure 4. Spectral response curves of alkali metal type photocathode on left and crystal type (right). ①Multialkali, ②Extended Multialkali, ③Bialkali, ④Cs-Te, ⑤GaAs, ⑥Extended GaAsP, ⑦GaAsP



# Lidar System Components

## Photo-detectors (I)

### PhotoMultiplier Tubes (PMTs) - Photocathode





# Lidar System Components

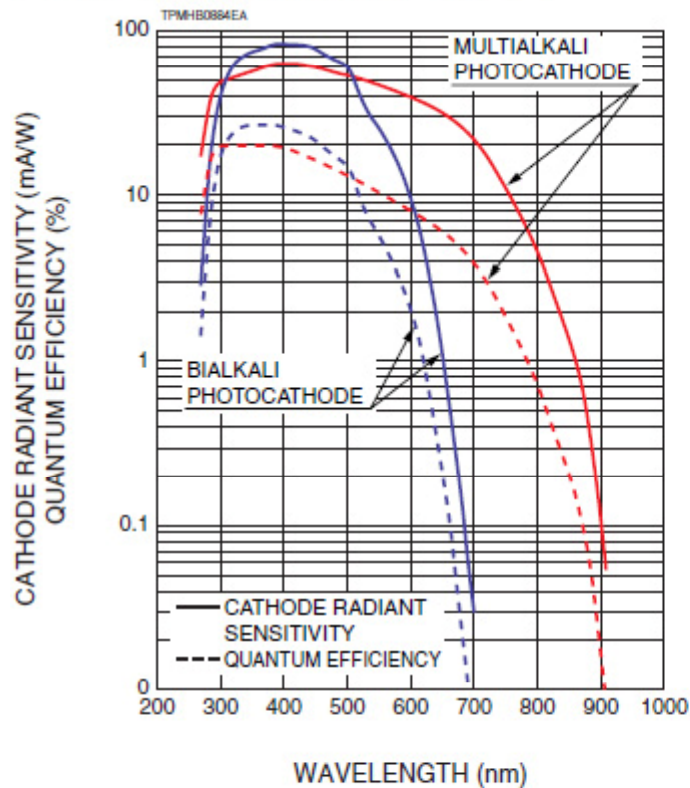
## Photo-detectors (I)

### PhotoMultiplier Tubes (PMTs) - Photocathode

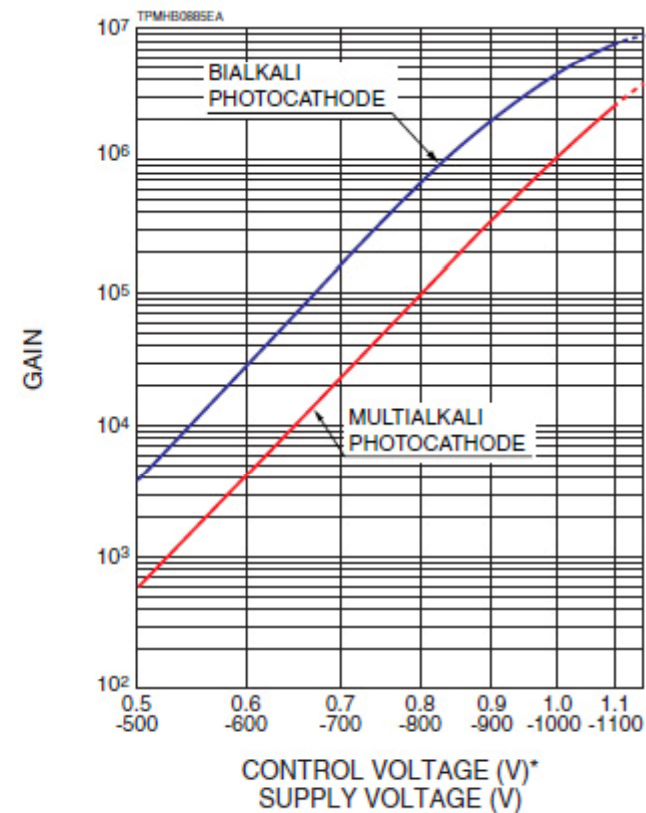
**Spectral response:** 1 photon (W)  $\rightarrow$  anode (mA)

**Gain:** 1 photon  $\rightarrow$  Nr photo-electrons ( $e^-$ )

#### ■ SPECTRAL RESPONSE



#### ■ GAIN

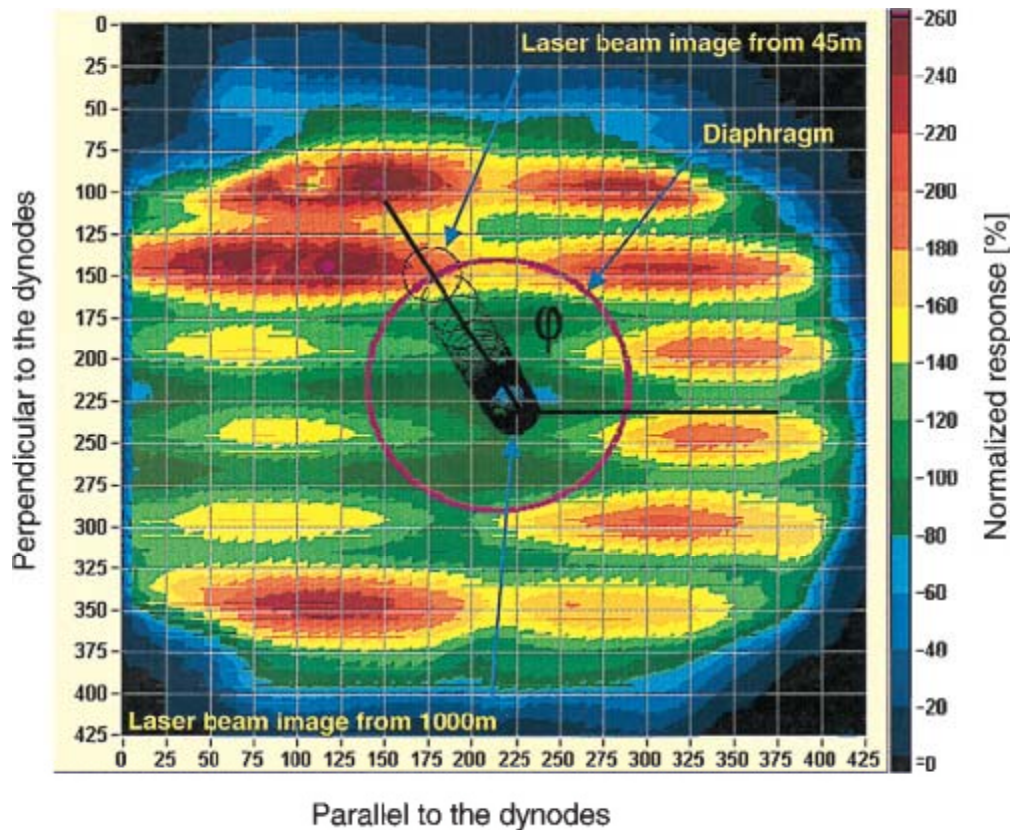


\* Control voltage of a Micro PMT module.

# Lidar System Components

## Photo-detectors (I)

### PhotoMultiplier Tubes (PMTs) – Spatial uniformity

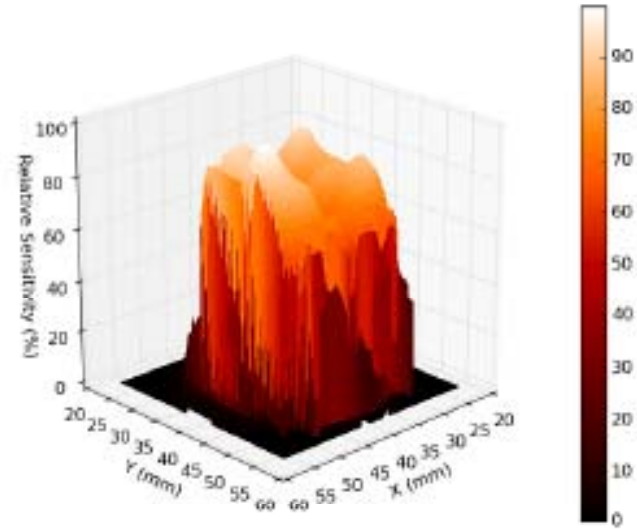
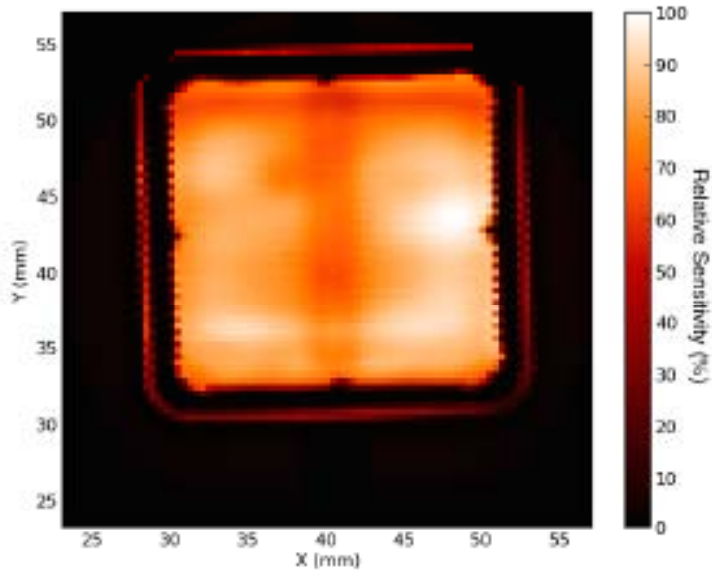


**Hint:** Always use doublet lenses in front of the PMTs to direct the light into a diam  $\sim$  3mm

# Lidar System Components

## Photo-detectors (I)

### PhotoMultiplier Tubes (PMTs) – Spatial uniformity



# Lidar System Components

## Photo-detectors (I)

### PhotoMultiplier Tubes (PMTs) – Anode collection space

The anode collection should have a suitable geometry for:

- collecting all secondary electrons emitted by the last dynode
- minimizing space charge effects to ensure **linear response in pulse-mode operation**
- matching the anode impedance to the characteristic impedance of the output connection (e.g, signal digitizer).

Anode sensitivity = Cathode sensitivity \* PMT Gain

# Lidar System Components

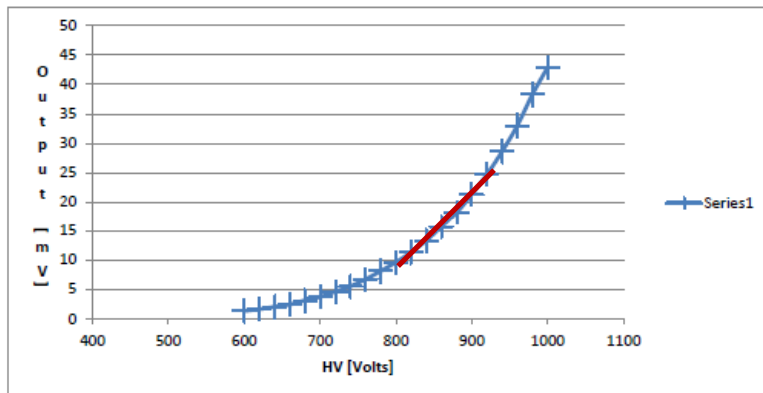
## Photo-detectors (I)

### PhotoMultiplier Tubes (PMTs) – Problems

- Never exceed the maximum average DC anode current ( $< 100 \mu\text{A}$ , or  $5\text{mV @}50\Omega$  input  $\rightarrow$  Atmospheric background !)
- Never exceed the maximum voltage ratings
- After pulses (spurious pulses at low signal levels):

Main causes:

- **Luminous reactions** (light emitted by the electrodes due to electron bombardment by high level light pulses)
- Ionization of residual traces gases
- PMT lifetime  $\sim 1/\text{number of incident photons } (N_{ip})$
- Change your PMT when its lifetime is exceeded !
- Linearity – Non linearity (Nr of electrons collected  $\sim$  Nr of incident pulses)



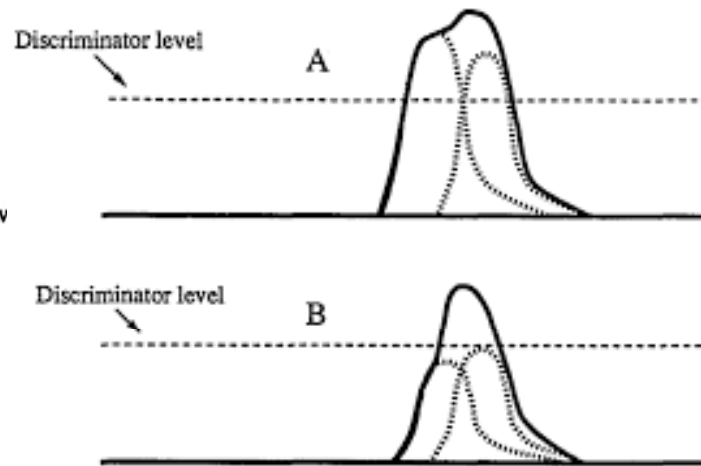
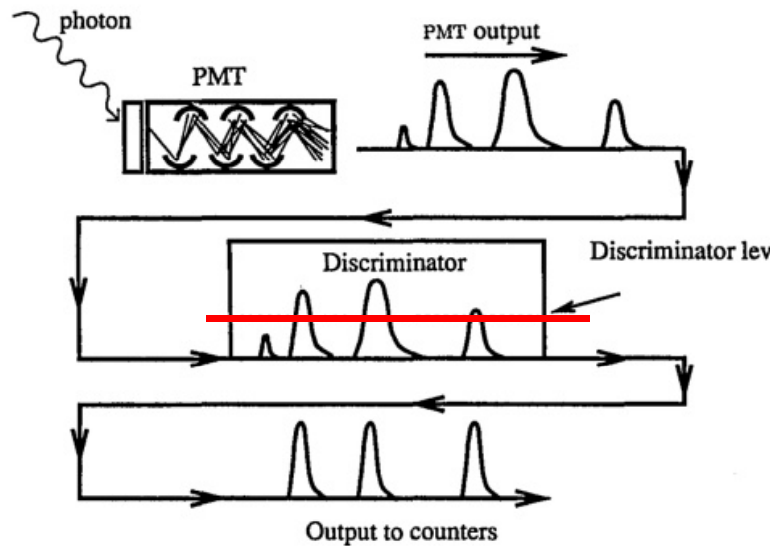
PMT Linear region (output vs HV,  
with const. light level input)

Kokkalis, PhD Thesis (2014)

# Lidar System Components

## Photo-detectors (I)

### PhotoMultiplier Tubes (PMTs) – Photon Counting mode



**Pulse pileup effect**

**A:** Count loss from pulse pileup

**B:** Count gain from pulse pileup

Donovan et al. (1993)



# Lidar System Components

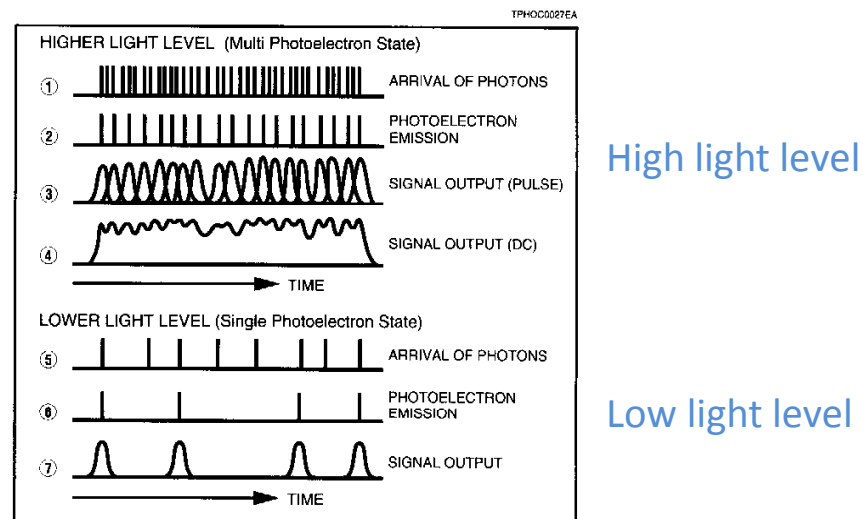
## Photo-detectors (I)

### PhotoMultiplier Tubes (PMTs) – Photon Counting mode

Photon counting regime:

**Low light level:** PMT responses **linearly** (the output signal is proportional to the incident light intensity),

**High light level:** PMT responses **NON-linearly** (the output signal is NOT proportional to the Incident light intensity) → overlapping of light pulses (pulse pileup effect)



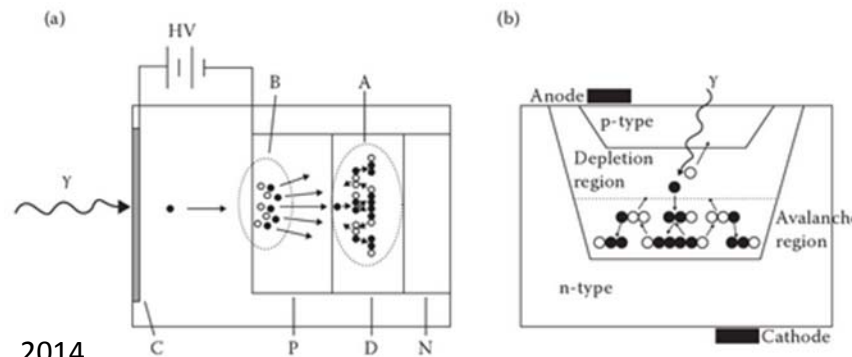
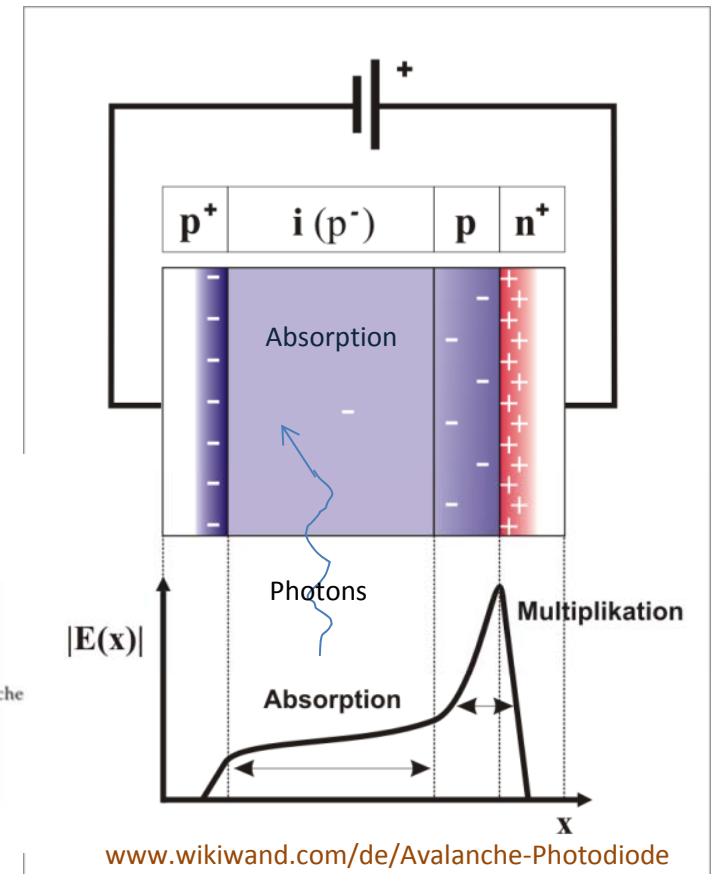
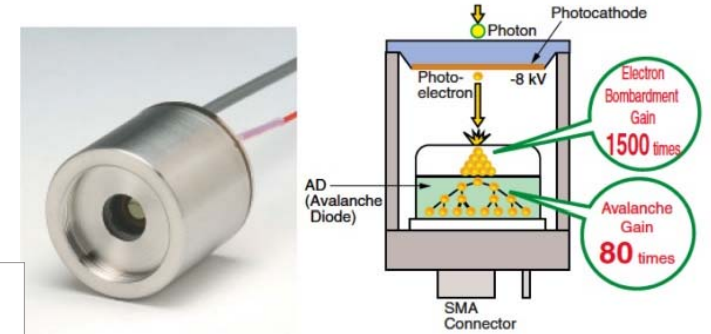
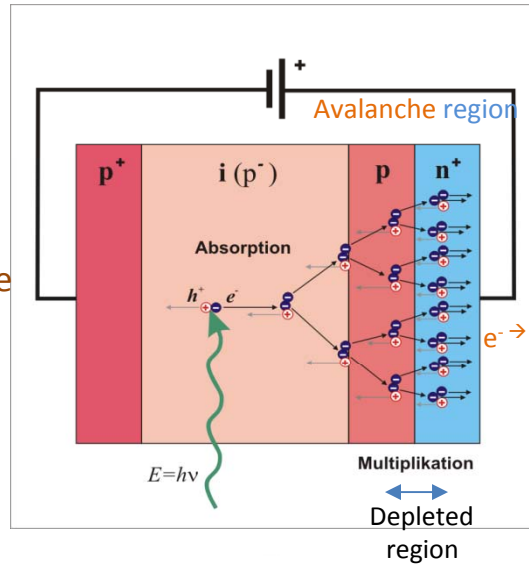
# Lidar System Components

## Photo-detectors (II)

### Avalanche PhotoDiodes (APDs)

- 1) Incident photons are **absorbed**
- 2) Electrons and holes are produced (p<sup>-</sup> region)
- 3) Electrons are accelerated (in the absorption region), thanks to E(x), collide with valence e<sup>-</sup> and, thus, produce free electrons (p region)
- 4) Electrons are accelerated, in the avalanche region, thanks to E(x) [100 kV/cm) , and produce secondary e<sup>-</sup> (depleted region) through impact ionization.

Reverse bias electric field



Marcu et al., 2014

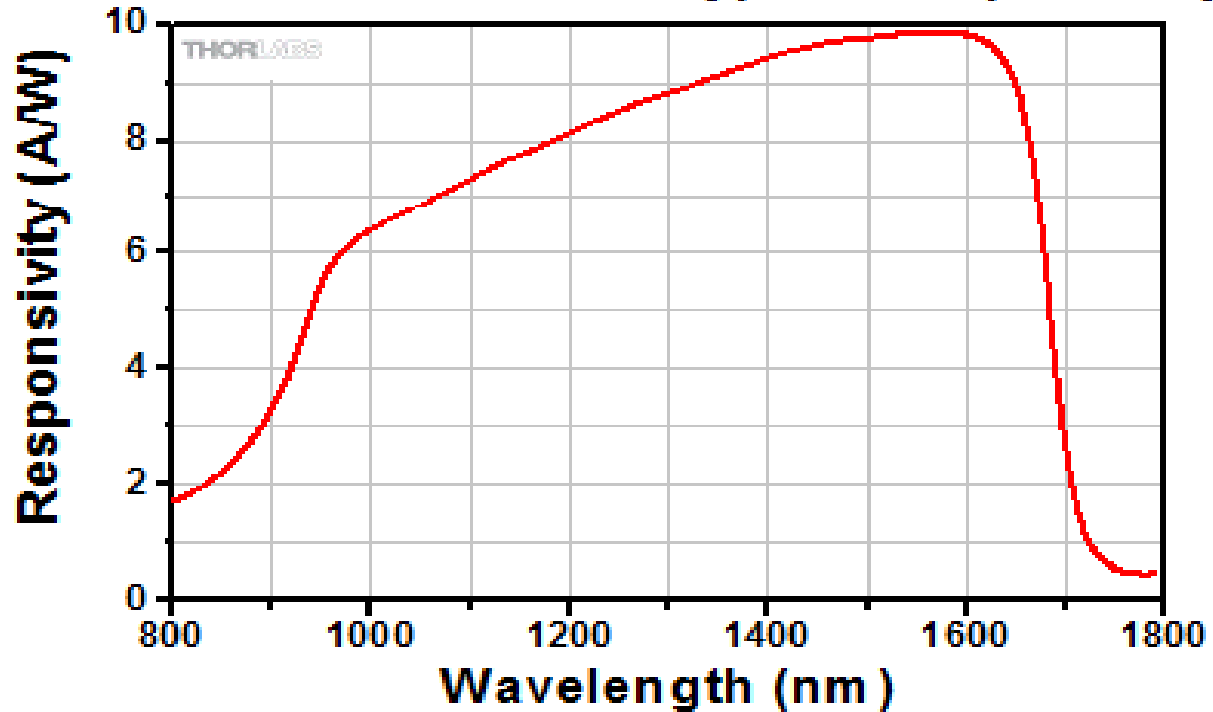
# Lidar System Components

## Photo-detectors (II)

### Avalanch PhotoDiodes (APDs)

**Spectral response:** 1 photon (W)  $\rightarrow$  anode (A)

**APD130C and APD110C Typical Responsivity**



# Lidar System Components

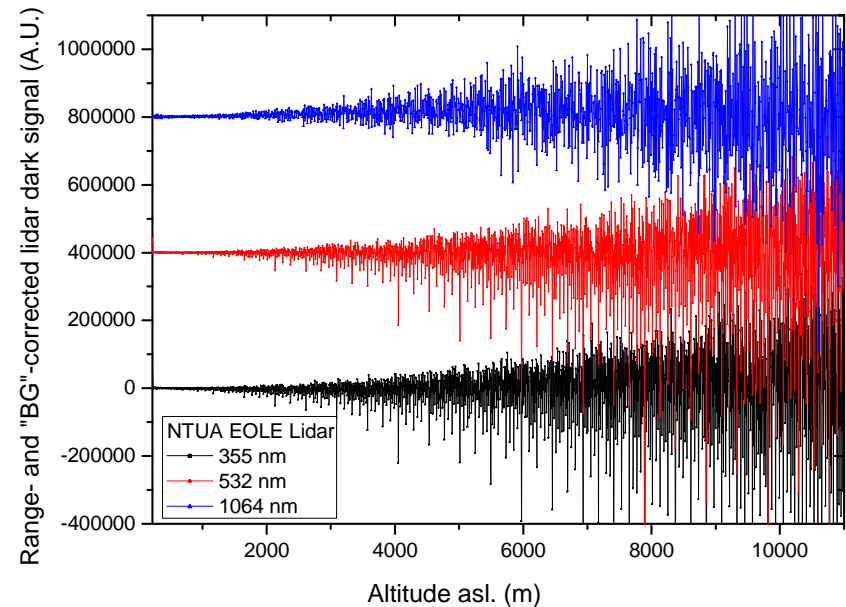
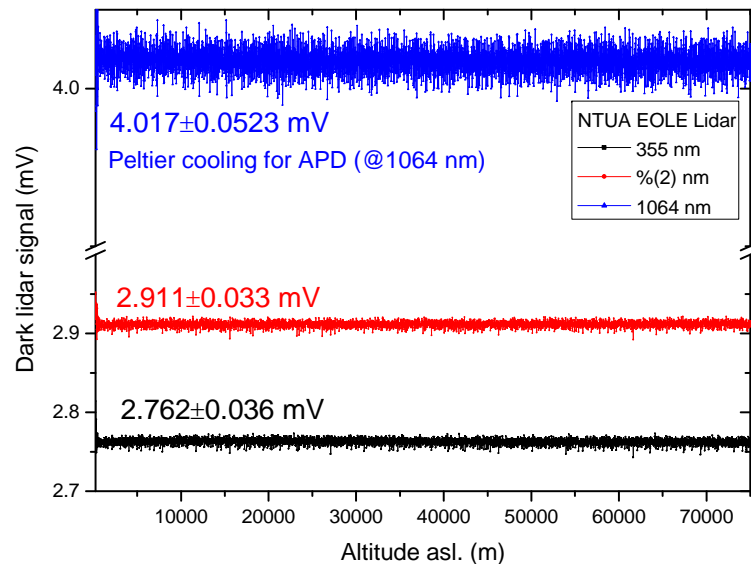
## Photo-detectors (I-II)

### PMTs - APDs– Anode dark current

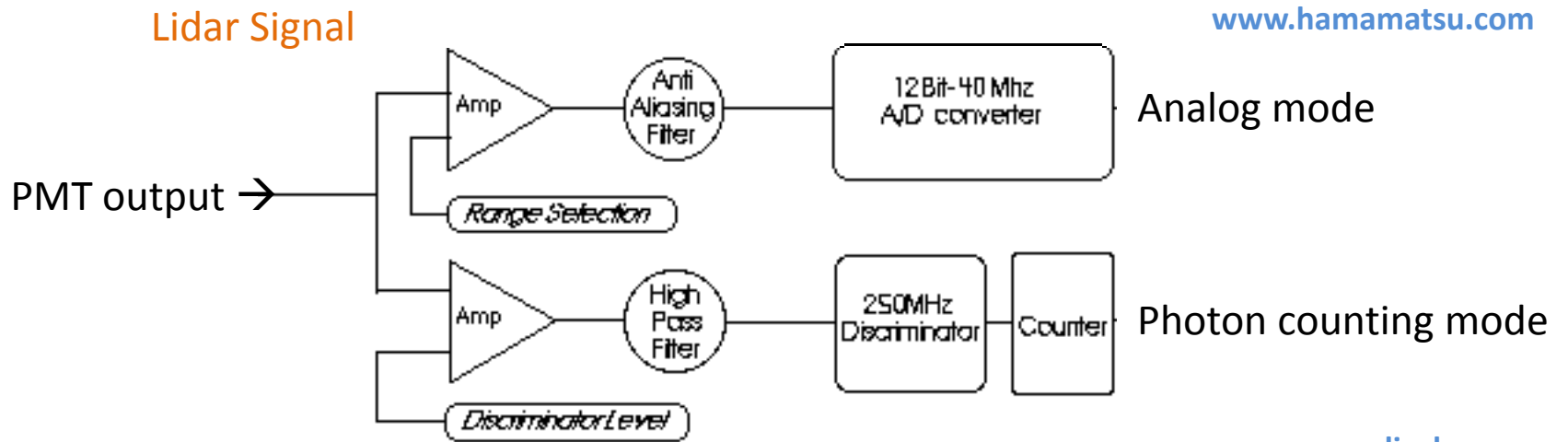
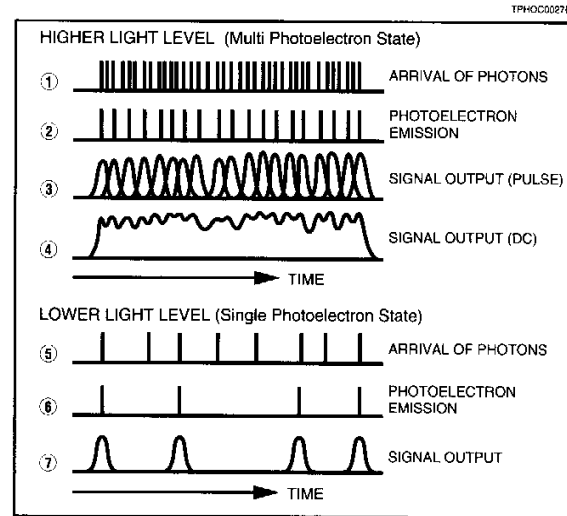
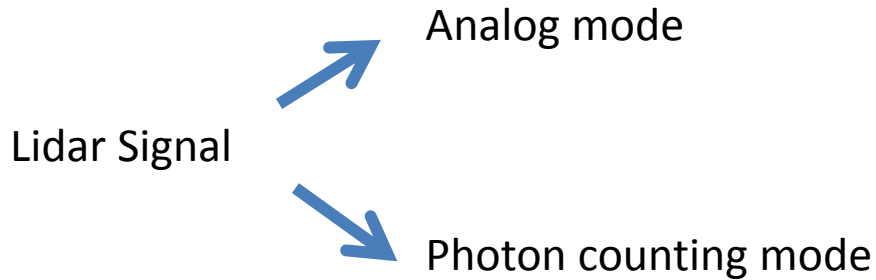
**Anode dark current** (in total darkness the PMT still produces a small output current)

- Ohmic leakage currents (leakage currents between electrodes and the glass)
- Thermionic current (thermionic emission of electrons from the photocathode)

NTUA, EOLE data



# Signal Detection



Analog to Digital Conversion (12-, 14-, 16-bit Digitizers)

# Signal ADC & Digitization/Sampling (Analog signals)

$\Delta t^* = 1/F_D$ ,  $F_D$  = Signal sampling frequency (10-40 MHz  $\rightarrow$   $\sim$  GHz)

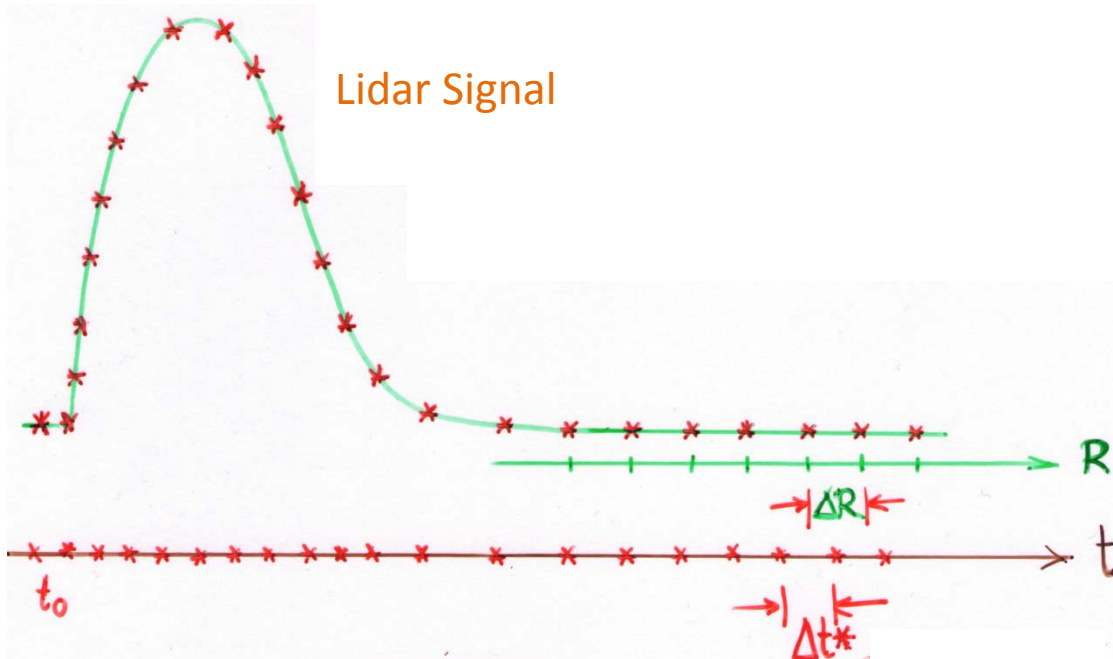
Example:

$F_D = 10$  MHz  $\rightarrow \Delta t^* = 100$  ns  $\rightarrow \Delta z = 15$  m

$F_D = 20$  MHz  $\rightarrow \Delta t^* = 50$  ns  $\rightarrow \Delta z = 7.5$  m

$F_D = 40$  MHz  $\rightarrow \Delta t^* = 25$  ns  $\rightarrow \Delta z = 3.75$  m

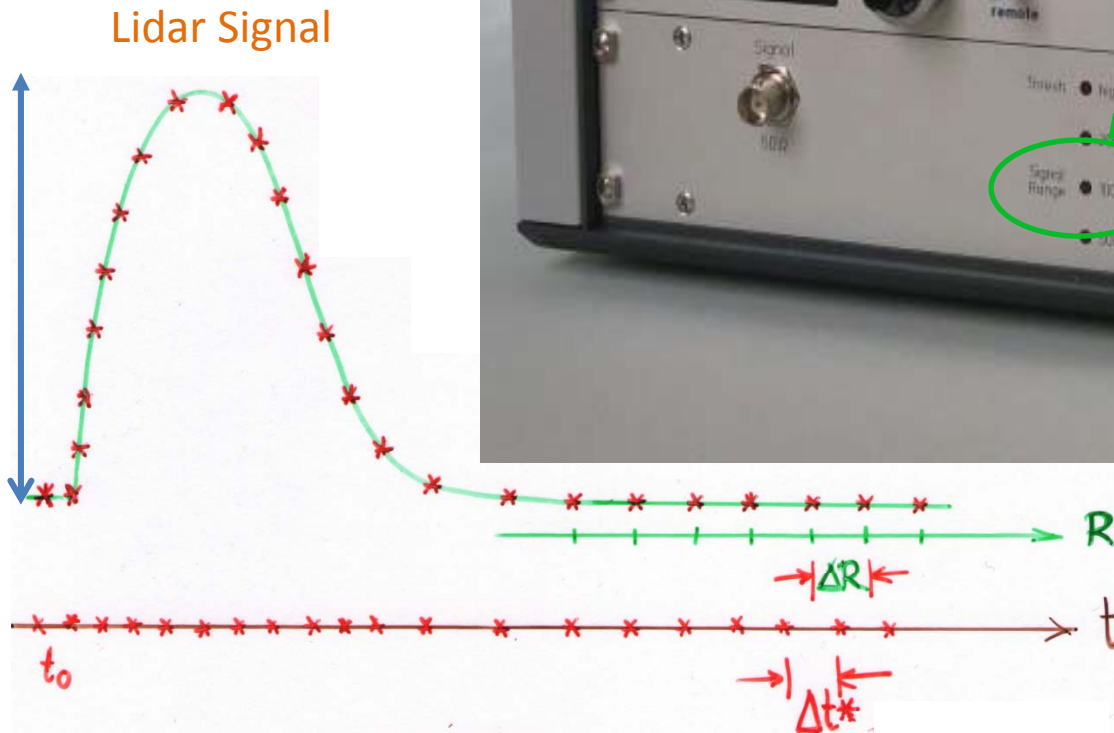
$F_D = 1$  GHz  $\rightarrow \Delta t^* = 1$  ns  $\rightarrow \Delta z = 0.15$  m





# Signal ADC & Digitization/Sampling (Analog signals)

**Rule of thumb:** Max Analog signal/2, e.g. for 40 mV input signal → **signal range** 100 mV



# Signal (Photon Counting mode)

Lidar Signal  $\longrightarrow$  Photon counting mode

## 3. NONPARALYZABLE SYSTEM

(Dead time correction)

$$(1) \quad N = \frac{S}{1 + S * \tau_d}$$

N - is the observed countrate

S - is the true countrate

$\tau_d$  - is the system dead time

While the paralyzable case is nonlinear equation, the nonparalyzable case can be easily inverted to

$$(2) \quad S = \frac{N}{1 - N * \tau_d}$$

As both cases are only a theoretical model, they are valid for lower countrates but fail when  $S * \tau_d$  becomes larger than one. From a numerical point of view Eq. 2 can be only applied to a signal as long as

$$(3) \quad N < \tau_d$$

For each PMT a dead time ( $\tau_d$ ) has to be measured !!

**Example:**

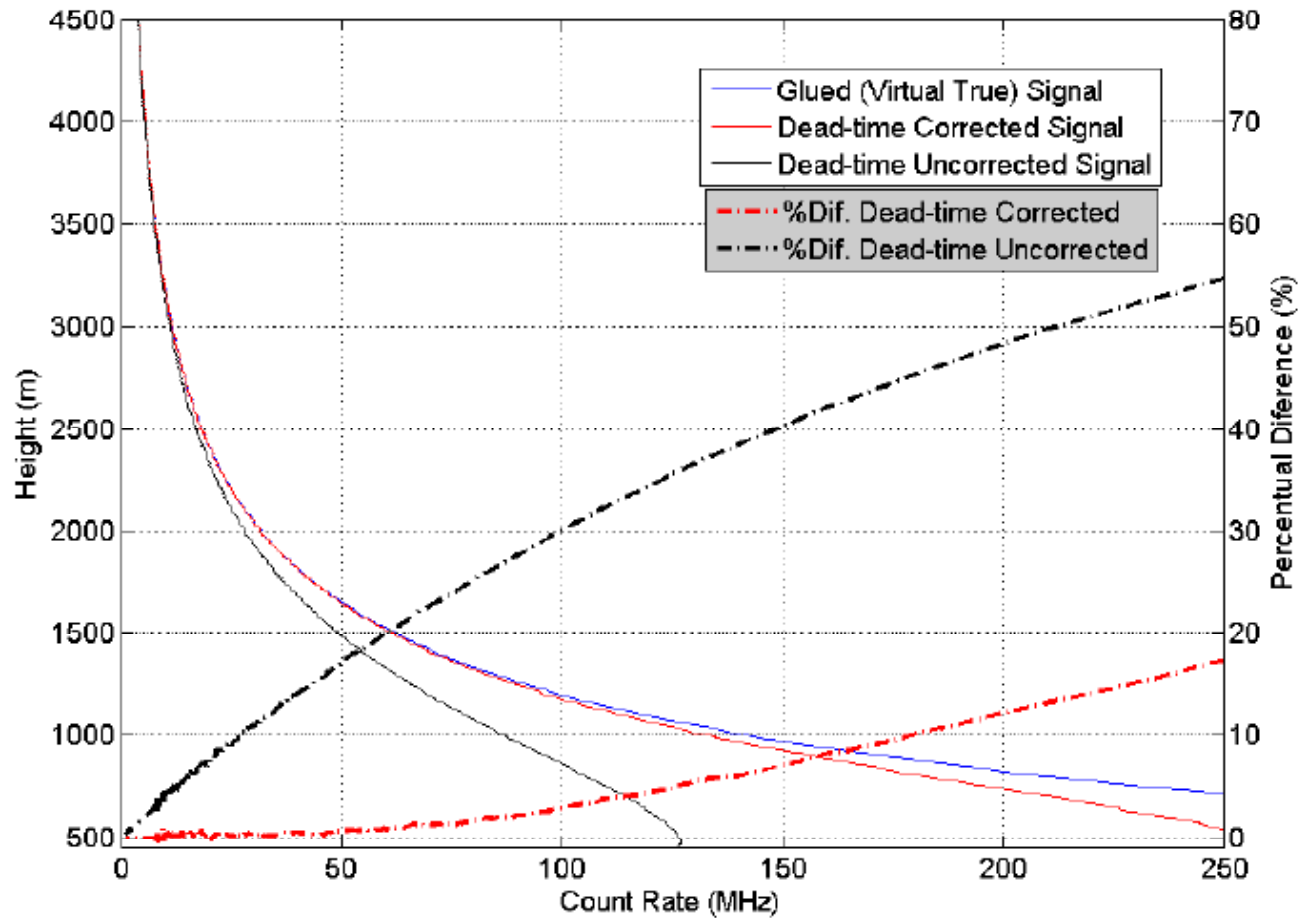
Alt= 0.5 km  $\rightarrow N_{\text{meas}}=50$  MHz,  $\tau_d=3.8$  ns  $\rightarrow S_{\text{true}}=61.75$  MHz

Alt= 3 km  $\rightarrow N_{\text{meas}}=10$  MHz,  $\tau_d=3.8$  ns  $\rightarrow S_{\text{true}}=10.4$  MHz

All photon counting signals (low altitudes) have to be corrected for dead time ( $N_{\text{meas}} > 10$  MHz)

# Signal (Photon Counting mode)

Lidar Signal → Photon counting mode (Dead time correction)



# Examples (I)

Data Preview and Analysis

D:\Midar\RAW\NTUA\Datalog.dat

ID	USER	LOCATION	START DATE	START TIME	STOP DATE	STOP TIME	
723	Vapor	Ath					RM0740709.455
724	Calipso	Athens	07/04/2007	09:45:50	07/04/2007	12:19:20	RM0740709.524
725	Vapor	Athens	12/04/2007	18:54:20	12/04/2007	20:58:10	RM0740709.592
726	Calipso	Athens	15/04/2007	23:11:10	16/04/2007	01:51:20	RM0740710.060
727	Aerosol	Athens	17/04/2007	09:07:40	17/04/2007	12:21:00	RM0740710.124
							RM0740710.192
							RM0740710.260
							RM0740710.324

File # 24  
Duration 02:40:00

User: All users  
Location: All Location  
Date: \*\*/\*\*

Change DB  
Edit Database  
Play  
Close

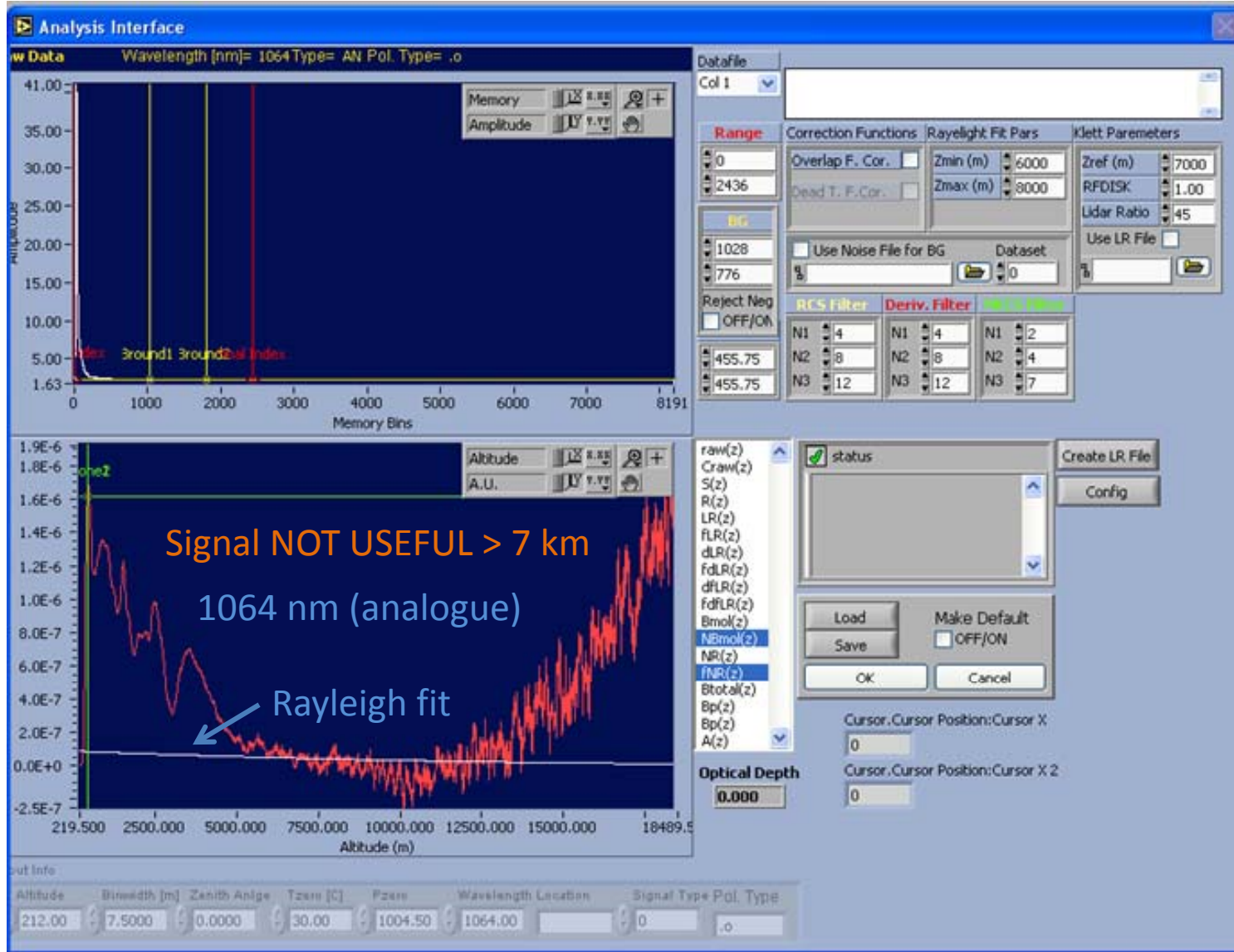
Shots#	Laser Fr.	Altitude=	Z. Angle=
0004000	0010	0200	28
0000000	0000	Longitude= 0023.0	Tzero= 17.0
		Latitude= 0037.0	Pzero= 1000.0

r. #	WaveL.	Pol. Type	Type	Scat. Type	Ch.#	Bw.	Distance	H. V	Shots.#	R/D(mV)
0	355.00	o	AN	Elastic	4000	15.00	52976.9	850	4000	0.500
0	355.00	o	PC	Elastic	4000	15.00	52976.9	850	4000	3.571
1	532.00	o	AN	Elastic	4000	15.00	52976.9	850	4000	0.500
1	532.00	o	PC	Elastic	4000	15.00	52976.9	850	4000	3.571
2	1064.00	o	AN	Elastic	4000	15.00	52976.9	305	4000	0.500

After a strong backscatter (from cloud) no useful signal remains

start | Analysis\_9\_12... | Microsoft Word | LabVIEW | Data Preview ... | 574 | 7:12 pm

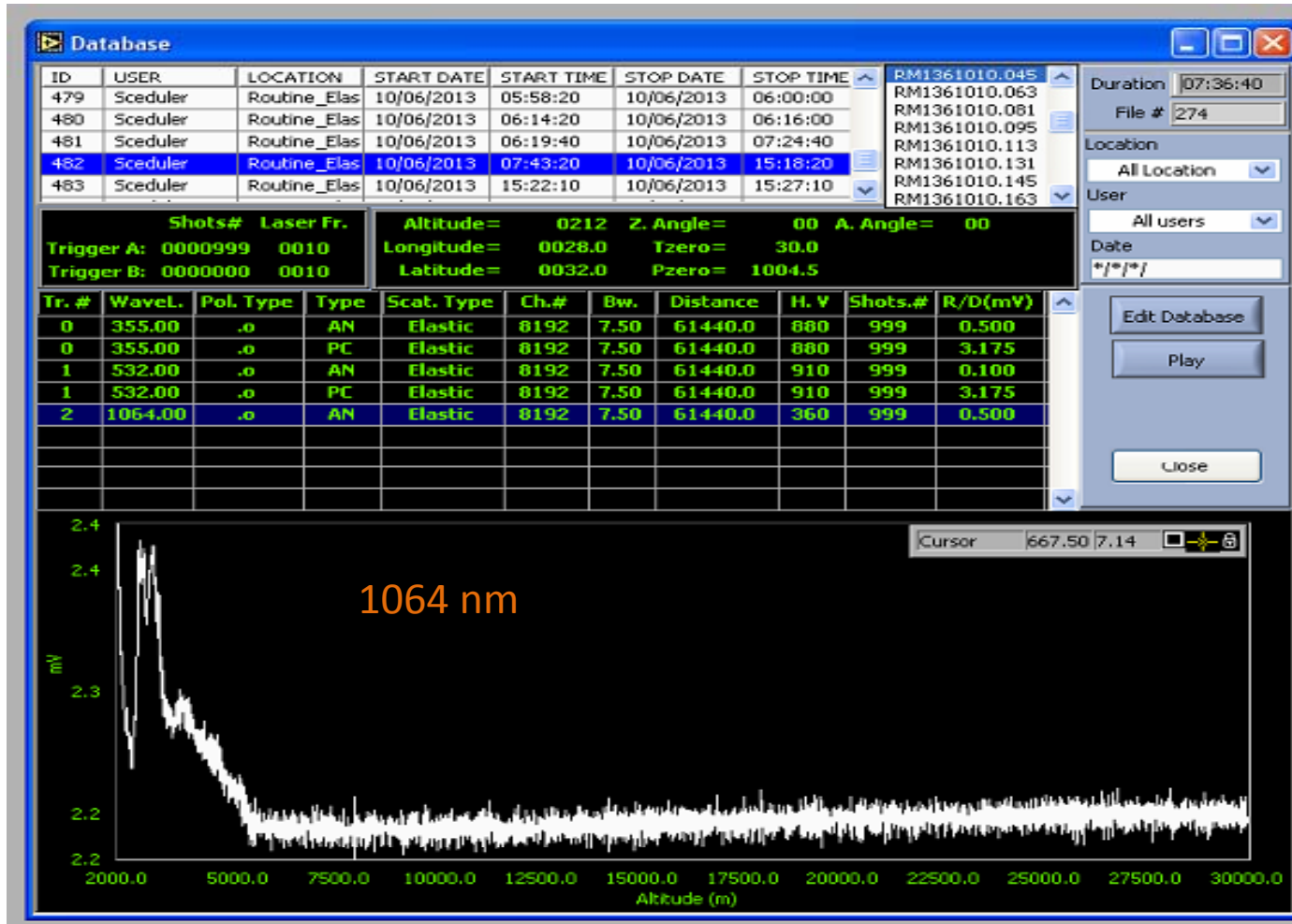
# Examples (II)



# Examples (III)

**PROBLEM : (not stable signal > 7 km height)**

Raw lidar signal with strong dust layer

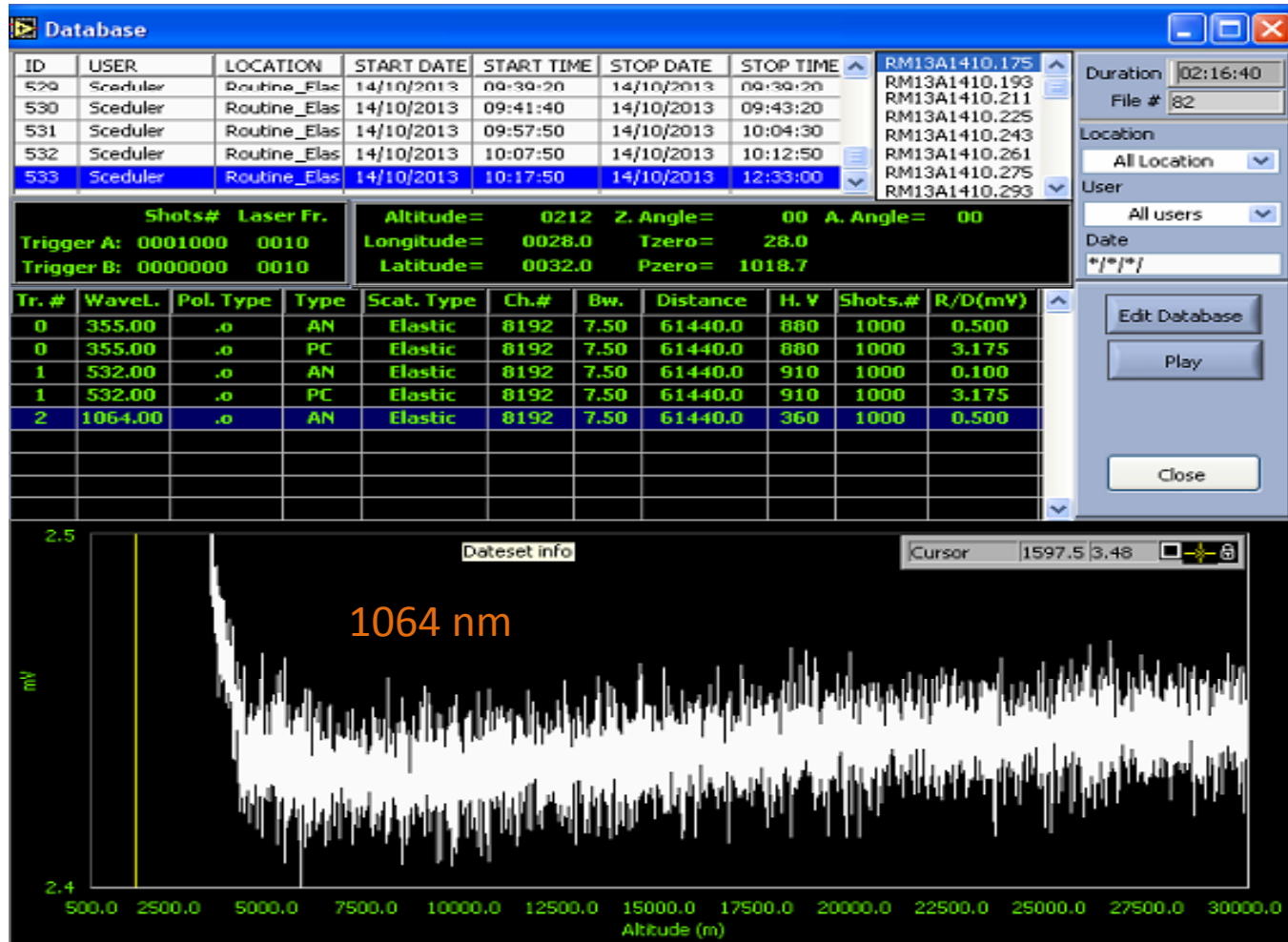


Problem due to not good earthing or too high HV



# Examples (IV)

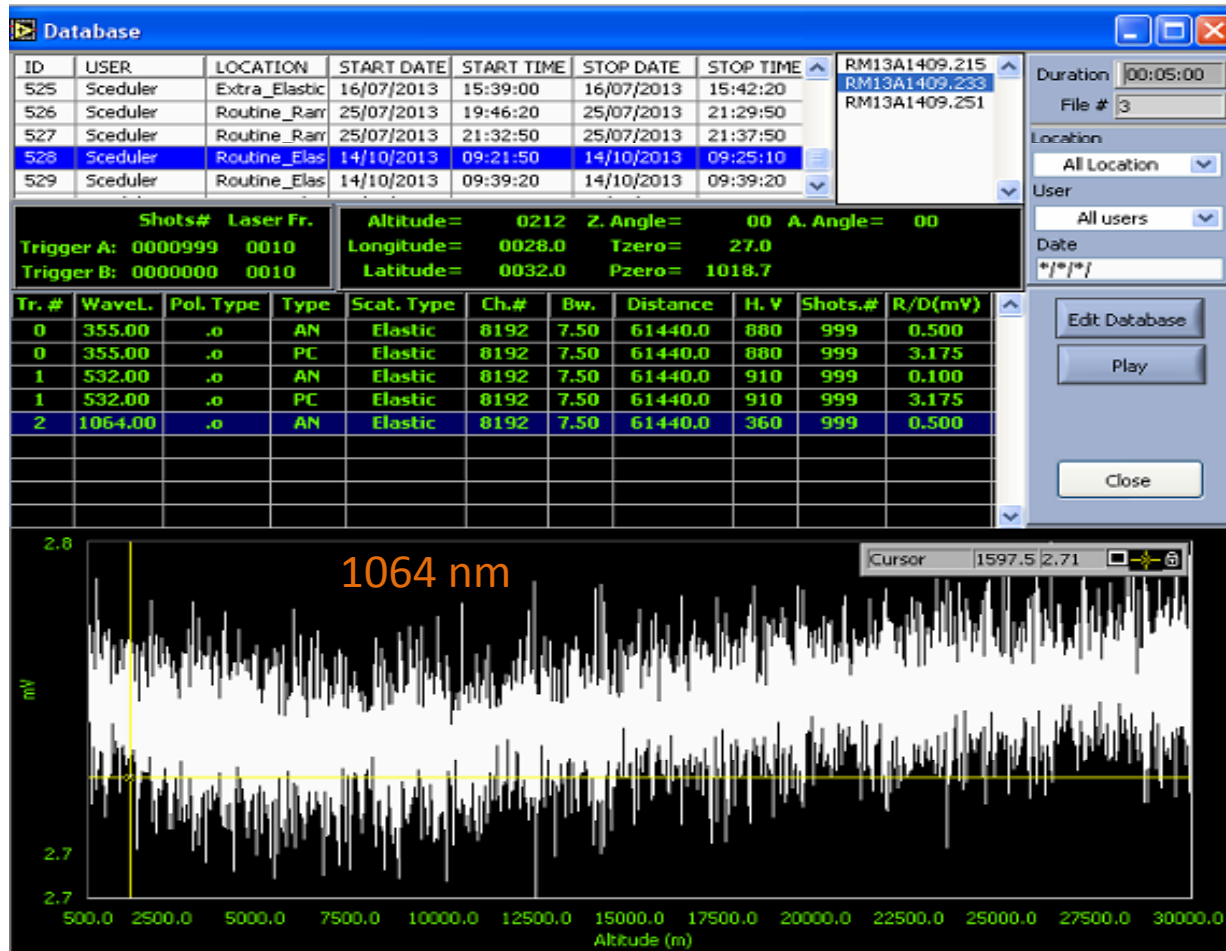
Raw lidar signal with dust layer



Problem due to not good earthing or too high HV

# Examples (V)

Noise file (dark file)



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Evangelatos, C., G. Tsaknakis, P. Bakopoulos, D. Papadopoulos, G. Avdikos, A. Papayannis, and G. Tzeremes, Q-switched laser with multi-segmented Nd:YAG crystal pumped at 885 nm for remote sensing, *Photonics Technology Letters* 26, 1890-1893, 2014.

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